## TEST REPORT EN 50549-1:2019

## Requirements for generating plants to be connected in parallel with distribution networks - Part 1-1: <br> Connection to a LV distribution network - Generating plants up to and including Type $\mathbf{B}$

| Report reference number ................: | 20TH0200-EN50549-1_0 |
| :--- | :--- |
| Date of issue.............................. : | 2020-01-14 |
| Total number of pages ....................... : | 105 |


| Ratings ....................................... : | ASW1000S-S | ASW1500S-S | ASW2000S-S | ASW3000S-S |
| :--- | :---: | :---: | :---: | :---: |
| MPP DC input voltage [V] ............... : | $80-550 \mathrm{Vdc}$ |  |  |  |
| Input DC voltage range [V].............. : | $80-580 \mathrm{Vdc}$ |  |  |  |
| Input DC current [A] ....................... : | $2 \times 12 \mathrm{~A}$ |  |  |  |
| Output AC voltage [V] ..................... : | $220 / 230 \mathrm{Vac}, 50 / 60 \mathrm{~Hz}$ |  |  |  |
| Output AC current [A]..................... : | Max.5,0 | Max.7,5 | Max.10,0 | Max. 13,6 |
| Nominal Output power [KW] ........... : | 1,000 | 1,500 | 2,000 | 3,000 |
| Max.Output apparent power [KVA].. : | 1,000 | 1,500 | 2,000 | 3,000 |


| Testing Location $\qquad$ <br> Address $\qquad$ | AISWEI New Energy Technology(Jiangsu) Co.,Ltd Building 9,No. 198 Xiangyang Road,215011 Suzhou,P.R.China |
| :---: | :---: |
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| Document History |  |  |  |
| :---: | :---: | :---: | :---: |
| Date | Internal reference | Modification / Change / Status | Revision |
| $2020-01-14$ | Weizhao Zheng | Initial report was written | 0 |
| Supplementary information: |  |  |  |

## Test items particulars

| Equipment mobility .......................: | Permanent connection |
| :---: | :---: |
| Operating condition .......................: | Continuous |
| Class of equipment .......................: | Class I |
| Protection against ingress of water... | IP65 according to EN 60529 |
| Mass of equipment [kg] .................. : | 6,5kg |
| Test case verdicts |  |
| Test case does not apply to the test object. | N/A |
| Test item does meet the requirement $\qquad$ | P (ass) |
| Test item does not meet the requirement $\qquad$ | F(ail) |
| Testing |  |
| Date of receipt of test item ..............: | 2019-11-01 |
| Date(s) of performance of test .........: | 2019-12-10 to 2020-01-08 |

## General remarks:

The test result presented in this report relate only to the object(s) tested. The report shall state compliance of the tested objects with the requirements of EN 50549-1. This report shall not be reproduced in part or in full without the written approval of the issuing testing laboratory.
"(see Annex \#)" refers to additional information appended to the report.
"(see appended table)" refers to a table appended to the report.
Throughout this report a comma is used as the decimal separator.

## This Test Report consists of the following documents:

1. Test Report
4.4 Normal operating range
4.5 Immunity to disturbances
4.6 Active response to frequency deviation
4.7 Power response to voltage variations and voltage changes
4.8 EMC and power quality
4.9 Interface protection
4.10 Connection and starting to generate electrical power
4.11 Ceasing and reduction of active power on set point
4.13 Requirements regarding single fault tolerance of interface protection system and interface switch
2. Annex No. 3 - Pictures of the unit
3. Annex No. 4 - Test equipment list

Copy of marking plate

| Model: ASW1000S-S |  |
| :---: | :---: |
| Max input voltage | d.c. 580 V |
| MPP voltage range | d.c. $80-550 \mathrm{~V}$ |
| Max. input current | d.c. 12 A |
| Isc PV(absolute maximum) | d.c. 18A |
| Rated grid voltage | a.c. $220 / 230 \mathrm{~V}$ |
| Rated grid frequency | $50 / 60 \mathrm{~Hz}$ |
| Max. AC output active power | 1000W |
| Max. AC output apparent power | 1000VA |
| Max.continuous output current | a.c. 5A |
| Adjustable $\cos (\phi)$ | 0.8ind...0.8cap |
| Operating temperature range | $-25 . . .460^{\circ} \mathrm{C}$ |
| Ingress protection | IP65 |
| Protective class | I |
| Overvoltage category | $\begin{array}{\|l\|} \hline \text { II(PV) } \\ \text { III(MAINS) } \\ \hline \end{array}$ |
| Supported DRMO,DRMS,DRMG,DRMT,D |  |
| AISWEI New Energy Technology (Jiangru) Ca., itd. Tat.: + 8651269370398 |  |
| $532-00443-00$ | Madein China |





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## General product information:

The Solar converter converts DC voltage into AC voltage.
The input and output are protected by Varistors to Earth. The unit is providing EMC filtering at the output toward mains. The unit does not provide galvanic separation from input to output (transformerless). The output is switched off redundant by the high power switching bridge and two relays. This assures that the opening of the output circuit will also operate in case of one error.
This unit is a single-phase inverter, that it is combine with operation mode. The inverter is able to generate power from solar modules to feed the grid(utility), also feed in the power to grid from the PV array.
The Solar converter provides with PV array of input.
The input of Solar converter can be supplied from PV array only.
Slip-mode frequency shift detection was used for LOM protection.

## Description of the electrical circuit:

The internal control is redundant built. It consists of Microcontroller Master DSP(U705) and Slave DSP(U710).
The Master DSP control the relays by switching signals; measures the PV voltage, PV current, Bus voltage, grid voltage, frequency, AC current with injected DC and the array insulation resistance to ground. In addition it tests the current sensors and the RCMU circuit before each start up.

The Slave DSP is measures the grid voltage, AC current, grid frequency and residual current, also can switch off the relays independently, and communicate with Master DSP each other.

The current is measured by a current sensor. The AC current signal and the injected DC current signal are sent to the Master DSP. The Master DSP tests and calibrates before each start up all current sensors.

The unit provides two relays in series in all output conductors. When single fault applied to one relay, alarm an error code on the mobile app or the upper computer, another redundant relay provides basic insulation maintained between the PV array and the mains. All the relays are tested before each start up. Both CPU can switch of the relays.


Figure 1 - Block diagram

## Differences of the models:

The models ASW1000S-S, ASW1500S-S, ASW2000S-S and ASW3000S-S are identical in hardware and software, and the output power derated by software.
The product was tested on:
Hardware: V1.0
Software: V1.0

All tests were performed on EUT of ASW3000S-S. Tests of the EUT of ASW3000S-S applicable for the models ASW1000S-S, ASW1500S-S and ASW2000S-S were performed on the concerned models and a statement is given at the relevant test.

## General remarks:

The test results presented in this report relate only to the object(s) tested.
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"(see Annex \#)" refers to additional information appended to the report.
"(see appended table)" refers to a table appended to the report.
Throughout this report a comma is used as the decimal separator.
The following suffixes are used for variables in tables and figures:

- " $\mathrm{P}_{\mathrm{n}}$ " for the nominal active power:

$$
P_{n}=U_{n} \times I_{n} \times \cos \varphi_{n} \text { (single-Phase); } P_{n}=\sqrt{ } 3 U_{n} x I_{n} \times \cos \varphi_{n} \text { (three-Phase) }
$$

- "Рм" for the momentary power
- "(c)" for over-excited
- "(i)" for under-excited


## Active and reactive power:

The regarded system of the voltage and current vectors is the load view (Figure 2):

- If the inverter feeds to the grid the active power is measured with negative sign. For the sake of reading the document the measured active infeed power has a positive sign

- If the inverter consumes inductive reactive power the reactive power is marked "inductive" or has a positive sign.
- If the inverter consumes capacitive reactive power the reactive power is marked "capacitive" or has a negative sign.


Figure 2

Default interface protection settings according EN 50549-1:2019:

| Parameter | Max. disconnection time | Min. operate time | Trip value |
| :--- | :---: | :---: | :---: |
| Over voltage - stage 1 | 3 s | $0,1 \mathrm{~s}$ | $230 \mathrm{~V}+10 \%(253 \mathrm{~V})$ |
| Over voltage - stage 2 | $0,2 \mathrm{~s}$ | $0,1 \mathrm{~s}$ | $230 \mathrm{~V}+15 \%(264,5 \mathrm{~V})$ |
| Under voltage | $1,5 \mathrm{~s}$ | $1,2 \mathrm{~s}$ | $230 \mathrm{~V}-15 \%(195,5 \mathrm{~V})$ |
| Over frequency | $0,5 \mathrm{~s}$ | $0,3 \mathrm{~s}$ | $52,0 \mathrm{~Hz}$ |
| Under frequency | $0,5 \mathrm{~s}$ | $0,3 \mathrm{~s}$ | $47,5 \mathrm{~Hz}$ |

An explicit Loss of Mains functionality shall be included. Established methods such as, but not limited to, Rate of Change of Frequency, Vector Shift or Source Impedance Measurement may be used. Where Source Impedance is measured, this shall be achieved by purely passive means, Any implementation which involves the injection of pulses onto the distribution network, shall not be permitted.

| ROCOF (where used) | 2 s |
| :--- | :---: |
| Reconnection settings for voltage | $0,85 \mathrm{U}_{\mathrm{n}} \leq \mathrm{U} \leq 1,10 \mathrm{U}_{\mathrm{n}}$ |
| Connection settings for frequency <br> (Normal operational start-up) | $49,5 \mathrm{~Hz} \leq \mathrm{f} \leq 50,1 \mathrm{~Hz}$ |
| Reconnection settings for frequency <br> (Automatic reconnection after tripping) | $49,5 \mathrm{~Hz} \leq \mathrm{f} \leq 50,2 \mathrm{~Hz}$ |
| Reconnection time | $\geq 60 \mathrm{~s}$ |
| Active power gradient after reconnection | $0,5 \%$ of rated inverter output current or 20mA |
| Permanent DC-injection | Inverter shall disconnect within 2 s. |
| Loss of mains according EN 62116 |  |

The stated currents and voltages are 'true r.m.s.'-values.
The voltages in this table are

- phase-to-neutral in 230 V single phase systems and 230/400 V systems,
- phase-to-phase in a multiphase 230 V system.

Tolerances on trip values:

- Voltage: $\pm 1 \%$ of $U_{n}$
- Frequency: $\pm 0,05 \mathrm{~Hz}$
- Disconnection time : $\pm 10 \%$

The following deviations for Poland, have been applied according the EN 50549-1:2019:

| Parameter | operate time | Trip value |
| :---: | :---: | :---: |
| ROCOF (where used) | 5 s | $0,4 \mathrm{~Hz} / \mathrm{s}$ |

An explicit Loss of Mains functionality shall be included. Established methods such as, but not limited to, Rate of Change of Frequency, Vector Shift or Source Impedance Measurement may be used. Where Source Impedance is measured, this shall be achieved by purely passive means, Any implementation which involves the injection of pulses onto the distribution network, shall not be permitted.

The stated currents and voltages are 'true r.m.s.'-values.
The voltages in this table are

- phase-to-neutral in 230 V single phase systems and $230 / 400 \mathrm{~V}$ systems,
- phase-to-phase in a multiphase 230 V system.

Tolerances on trip values:

- Voltage: $\pm 1 \%$ of $U_{n}$
- Frequency: $\pm 0,05 \mathrm{~Hz}$
- Disconnection time : $\pm 10 \%$


## EN 50549:2019, clause 4: Tests

| Clause | Test requirement (According to table C.1) | Result |
| :--- | :--- | :---: |
| 4.4 | Normal operating range | $\mathbf{P}$ |
| 4.5 | Immunity to disturbances | $\mathbf{P}$ |
| 4.6 | Active response to frequency deviation | $\mathbf{P}$ |
| 4.7 | Power response to voltage variations and voltage changes | $\mathbf{P}$ |
| 4.8 | EMC and power quality | $\mathbf{P}$ |
| 4.9 | Interface protection | $\mathbf{P}$ |
| 4.10 | Connection and starting to generate electrical power | $\mathbf{P}$ |
| 4.11 | Ceasing and reduction of active power on set point | $\mathbf{P}$ |
| 4.12 | Remote information exchange | N/A |
| 4.13 | Requirements regarding single fault tolerance of interface protection system and <br> interface switch | $\mathbf{P}$ |

## EN 50549-1:2019: Normal operating range

| Clause | Test requirement | Test procedure according standard | Result |
| :--- | :--- | :--- | :---: |
| 4.4 .2 | Power response to over-frequency | EN 50438, Annex D.3.1 | P |
| 4.4 .3 | Power response to under-frequency | G99/1-4, clause A.7.3.2 | P |
| 4.4 .4 | Continuous operating voltage range | EN 50438, Annex D.3.1 | P |


| $\begin{array}{ll}\text { 4.4.2 } & \text { Operating frequency range } \\ \text { 4.4.4 } & \text { Continuous operating voltage range }\end{array}$ |  |  |  |  | P |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Setting values |  | Over-voltage [V]: | 253 |  |  |
|  |  | Under-voltage [V]: | 195,5 |  |  |
|  |  | Over-frequency [Hz]: | 51,5 |  |  |
|  |  | Under-frequency [Hz]: | 47,5 |  |  |
|  |  |  |  |  |  |
| Test result: |  |  |  |  |  |
| Test sequence | Voltage [V] | Frequency [ Hz ] | Output power [kW] | $\operatorname{Cos} \varphi$ |  |
| Test1 | 195,59 | 47,50 | 2,672 | 0,9985 |  |
| Test2 | 195,59 | 48,50 | 2,672 | 0,9985 |  |
| Test3 | 253,19 | 51,50 | 3,000 | 0,9999 |  |
| Test4 | 230,48 | 50,00 | 3,012 | 0,9999 |  |
| Test5 | 230,08 | 50,50 | 3,007 | 0,9988 |  |
| Note: <br> Test method refer clause D.3.1 of EN 50438:2013. <br> During the tests the interface protection was disabled. <br> Operation at reduced power is allowed during test 1 , equal to the maximum power that can be supplied on reaching the maximum output current limit ( $\mathrm{P} \geq 0,85 \mathrm{~S}_{\mathrm{n}}$ ). <br> During the sequence of test 3 , automatic adjustment to reduce power in the case of over-frequency was disabled. <br> The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software. |  |  |  |  |  |



## Test result:

|  | Switch to: |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| 5-min mean value (each) | a) $49,50 \mathrm{~Hz}$ | b) $49,00 \mathrm{~Hz}$ | c) $48,00 \mathrm{~Hz}$ | d) $47,60 \mathrm{~Hz}$ | e) $47,10 \mathrm{~Hz}$ |
| Frequency [Hz]: | 49,50 | 49,00 | 48,00 | 47,60 | 47,10 |
| Active power [kW]: | 3,006 | 3,006 | 3,005 | 3,004 | 3,005 |
| $\Delta \mathrm{P} / \mathrm{P}_{\mathrm{n}}[\%]:$ | 0,205 | 0,197 | 0,178 | 0,149 | 0,169 |

## Assessment criterion:

Test method refer clause A.7.3.2 of G99/1-4
The frequency should then be set to $49,5 \mathrm{~Hz}$ for 5 minutes. The output should remain at $100 \%$ of registered Capacity.
The frequency should then be set to $49,0 \mathrm{~Hz}$ and once the output has stabilised, held at this frequency for 5 minutes. The Active Power output must not be below 99\% of registered Capacity.
The frequency should then be set to $48,0 \mathrm{~Hz}$ and once the output has stabilised, held at this frequency for 5 minutes. The Active Power output must not be below 97\% of registered Capacity.
The frequency should then be set to $47,6 \mathrm{~Hz}$ and once the output has stabilised, held at this frequency for 5 minutes. The Active Power output must not be below $96.2 \%$ of registered Capacity.
The frequency should then be set to $47,1 \mathrm{~Hz}$ and held at this frequency for 20 s . The Active Power output must not be below $95,0 \%$ of registered Capacity and the Synchronous Power Generating Module must not trip in less than the 20 s of the test.


Maximum allowable power reduction in case of under-frequency

## Note:

The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.

| EN 50549-1:2019: Immunity to disturbances |  |  |  |
| :--- | :--- | :--- | :---: |
| Clause | Test requirement | Test procedure according standard | Result |
| 4.5 .2 | Rate of change of frequency (RoCoF) <br> immunity | G99/1-4:2019, clause A.7.1.2.6 | P |
| 4.5 .3 | Low voltage ride through (LVRT) | VDE V 0124-100:2019-02 (Draft), clause <br> 5.8 .3. | P |
| 4.5 .4 | High voltage ride through (HVRT) | VDE V 0124-100:2019-02 (Draft), clause <br> 5.8 .3. | P |
| 4.7 .4 | Zero current mode for converter <br> connected generating plants | VDE V 0124-100:2019-02 (Draft), clause <br> 5.8 .3. | $\mathbf{P}$ |


| 4.5.2 Rate of change of frequency (ROCOF) immunity | P |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  | Start Frequency | Change | End Frequency | Confirm no trip |
|  | 49 Hz | $+2 \mathrm{~Hz} / \mathrm{sec}$ | 51 Hz | No trip |
| Positive Frequency drift | 51 Hz | $-2 \mathrm{~Hz} / \mathrm{sec}$ | 49 Hz | No trip |
| Negative Frequency drift |  |  |  |  |

## Note:

Test method refer clause A.7.1.2.6 of G99/1-4:2019.
Hold for 10 s
Manufacturers considering new designs should allow for the RoCoF where stability is required to be increased to, up to 2 Hz per second, as proposed in the new European network codes, which are expected to come into force over the period 2014/2015. Under these conditions RoCoF will cease to be an effective loss of mains protection and is unlikely to be permitted in future revisions of this document.
For the step change test the SSEG should be operated with a measureable output at the start frequency and then a vector shift should be applied by extending or reducing the time of a single cycle with subsequent cycles returning to the start frequency. The start frequency should then be maintained for a period of at least 10 seconds to complete the test. The SSEG should not trip during this test.
For frequency drift tests the SSEG should be operated with a measureable output at the start frequency and then the frequency changed in a ramp function at $0,95 \mathrm{~Hz}$ per second to the end frequency. On reaching the end frequency it should be maintained for a period of at least10 seconds. The SSEG should not trip during this test.
The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.

| 4.5.3 | Low voltage ride through (LVRT) | P |
| :--- | :--- | :--- |
| 4.5.4 | High voltage ride through (HVRT) |  |
| 4.7.4 | Zero current mode for converter connected generating plants |  |

## General:

If the voltage on the generator terminals falls below $<0.8 U_{n}$ and if the generator terminals exceed the voltage of $>1.15 \mathrm{U}_{\mathrm{n}}$ (start of fault), generator must pass through voltage dips without any current being drawn into the grid Network operator (limited dynamic network support).
This requirement is met if, for a voltage dip below $0.8 \mathrm{U}_{\mathrm{n}}$ or at a voltage increase above $1.15 \mathrm{U}_{\mathrm{n}}$, the injected current of the generating unit (s) and / or the memory 60 ms after occurrence of this voltage dip in any outer conductor $20 \%$ of the rated current $\mathrm{I}_{r}$ and does not exceed> $10 \% \mathrm{I}_{r}$ after 100 ms .
After the voltage returned to continuous operating voltage range of $-15 \% U_{n}$ to $+10 \% U_{n}, 90 \%$ of pre fault power or available power whichever is the smallest shall be resumed as fast as possible, but at the latest within 1 s unless the DSO and the responsible party requires another value.


Figure 6 - Low voltage ride through capability for non-synchronous generating technology


Figure 8 - Over-voltage ride through capability

| BUREAU |
| :--- |
| VERITAS |


| Test | Drop depth requirement [p.u. $U_{n}$ ] | Symmetry | Fault duration [ms] | Output power level |  | k-factor | Test no. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | P set point <br> ( $\left.\mathrm{Pre}_{\mathrm{r}} / \mathrm{p} . \mathrm{u}.\right)$ | Q set point (Q / p.u.) |  |  |
| 1.A. 1 | 0,05 | Symmetrical | 250 | 1,0 | 0,00 | 2 | 1.A. 1 |
| 1.A. 2 |  |  |  | 0,2 |  |  | 1.A. 2 |
| 1.D. 1 |  |  |  | 1,0 |  |  | 1.D. 1 |
| 1.D. 2 |  |  |  | 0,2 |  |  | 1.D. 2 |
| 1.B. 1 |  | Single phase* |  | 1,0 |  |  | 1.B. 1 |
| 1.B. 2 |  |  |  | 0,2 |  |  | 1.B. 2 |
| 2.A. 1 | 0,31 | Symmetrical | 1300 | 1,0 | 0,00 | 2 | 2.A. 1 |
| 2.A. 2 |  |  |  | 0,2 |  |  | 2.A. 2 |
| 2.D. 1 |  |  |  | 1,0 |  |  | 2.D. 1 |
| 2.D. 2 |  |  |  | 0,2 |  |  | 2.D. 2 |
| 2.B. 1 |  | Single phase* |  | 1,0 |  |  | 2.B. 1 |
| 2.B. 2 |  |  |  | 0,2 |  |  | 2.B. 2 |
| 3.A. 1 | 0,85 | Symmetrical | 3000 | 1,0 | 0,00 | 2 | 3.A. 1 |
| 3.A. 2 |  |  |  | 0,2 |  |  | 3.A. 2 |
| 3.D. 1 |  |  |  | 1,0 |  |  | 3.D. 1 |
| 3.D. 2 |  |  |  | 0,2 |  |  | 3.D. 2 |
| 3.B. 1 |  | Single phase* |  | 1,0 |  |  | 3.B. 1 |
| 3.B. 2 |  |  |  | 0,2 |  |  | 3.B. 2 |
| OV1 | 1,25 | Symmetrical | 100 | 1,0 | 0,00 | 2 | OV1 |
| OV2 | 1,20 |  | 5000 | 1,0 |  |  | OV2 |
| OV3 | 1,15 |  | 60000 | 1,0 |  |  | OV3 |

Note:
For every kind of voltage dip a test without load has to be performed in order to prove that the test condition was fulfilled. The voltage has to drop to AT LEAST the defined depth level. An exception can be considered in case no current is supplied during dips.

## * Single phase = "choose Typ 7 at BV-Lab Studio" $\hat{=}$ LVRT Typ B

## Graph of FRT test one

## Test result:

| List of tests | Residual amplitude of phase-to-phase voltage [p.u. $\mathrm{U}_{\mathrm{n}}$ ] | Duration limit [ms] | Duration [ms] | Result |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{Pemax}_{\text {min }}$ \% | 20\% $\pm 5 \%$ |  |  |  |
| 1.D.1- Asymmetrical fault phase [Phase 1] | 0,05 | $250 \pm 20$ | 251 | Pass |
| 1.D.1- Asymmetrical fault phase [Phase 2] | 0,05 | $250 \pm 20$ | 250 | Pass |
| 1.D.1-Asymmetrical fault phase [Phase 3] | 0,05 | $250 \pm 20$ | 250 | Pass |
| 2.D.1- Asymmetrical fault phase [Phase 1] | 0,31 | $1300 \pm 20$ | 1300 | Pass |
| 2.D.1-Asymmetrical fault phase [Phase 2] | 0,31 | $1300 \pm 20$ | 1300 | Pass |
| 2.D.1- Asymmetrical fault phase [Phase 3] | 0,31 | $1300 \pm 20$ | 1300 | Pass |
| 3.D.1-Asymmetrical fault phase [Phase 1] | 0,85 | $3000 \pm 20$ | 3000 | Pass |
| 3.D.1-Asymmetrical fault phase [Phase 2] | 0,85 | $3000 \pm 20$ | 3000 | Pass |
| 3.D.1-Asymmetrical fault phase [Phase 3] | 0,85 | $3000 \pm 20$ | 3000 | Pass |
| $\mathrm{Pemax}_{\text {in }}$ \% | 100\% $\pm 5 \%$ |  |  |  |
| 1.D.2- Asymmetrical fault phase [Phase 1] | 0,05 | $250 \pm 20$ | 250 | Pass |
| 1.D.2- Asymmetrical fault phase [Phase 2] | 0,05 | $250 \pm 20$ | 251 | Pass |
| 1.D.2- Asymmetrical fault phase [Phase 3] | 0,05 | $250 \pm 20$ | 250 | Pass |
| 2.D.2- Asymmetrical fault phase [Phase 1] | 0,31 | $1300 \pm 20$ | 1300 | Pass |
| 2.D.2- Asymmetrical fault phase [Phase 2] | 0,31 | $1300 \pm 20$ | 1300 | Pass |
| 2.D.2- Asymmetrical fault phase [Phase 3] | 0,31 | $1300 \pm 20$ | 1300 | Pass |
| 3.D.2- Asymmetrical fault phase [Phase 1] | 0,85 | $3000 \pm 20$ | 3000 | Pass |
| 3.D.2- Asymmetrical fault phase [Phase 2] | 0,85 | $3000 \pm 20$ | 3000 | Pass |
| 3.D.2- Asymmetrical fault phase [Phase 3] | 0,85 | $3000 \pm 20$ | 3000 | Pass |
| OV1- Symmetrical fault phase | 1,25 | $100 \pm 20$ | 101 | Pass |
| OV2- Symmetrical fault phase | 1,20 | $5000 \pm 20$ | 5000 | Pass |
| OV3- Symmetrical fault phase | 1,15 | $60000 \pm 20$ | 60000 | Pass |

## Graph of FRT test one

Test result:

| List of tests | Residual amplitude of <br> phase-to-phase voltage <br> $\left[\mathrm{p} . \mathrm{u} . \mathrm{U}_{\mathrm{n}}\right]$ | Duration limit [ms] | Duration <br> $[\mathrm{ms}]$ | Result |
| :---: | :---: | :---: | :---: | :---: |

## Test conditions:

Voltage simulator fall and rise time: < 20ms
Used sample rate: 10 kHz

## Note:

The test method refer to VDE V 0124-100:2019-02 (Draft), clause 5.8.3.
The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.

## Test 1: 1.D.1- Asymmetrical fault phase [Phase 1]; $P=20 \% \pm 5 \% P_{n}$



Test 1: 1.D.1- Asymmetrical fault phase [Phase 2]; $P=20 \% \pm 5 \% P_{n}$


## Test 1: 1.D.1- Asymmetrical fault phase [Phase 3]; $P=20 \% \pm 5 \% P_{n}$



Test 2: 2.D.1- Asymmetrical fault phase [Phase 1]; $\mathbf{P = 2 0 \%} \pm 5 \% \mathbf{P}_{\mathrm{n}}$


## Test 2: 2.D.1- Asymmetrical fault phase [Phase 2]; $\mathrm{P}=\mathbf{2 0 \%} \pm 5 \% \mathrm{P}_{\mathrm{n}}$



Test 2: 2.D.1- Asymmetrical fault phase [Phase 3]; $P=20 \% \pm 5 \% P_{n}$


## Test 3: 3.D.1- Asymmetrical fault phase [Phase 1]; $\mathbf{P = 2 0 \% ~} \pm 5 \% \mathbf{P}_{\mathrm{n}}$



Test 3: 3.D.1- Asymmetrical fault phase [Phase 2]; $P=20 \% \pm 5 \% P_{n}$


## Test 3: 3.D.1- Asymmetrical fault phase [Phase 3]; $P=20 \% \pm 5 \% P_{n}$



Test 1: 1.D.2- Asymmetrical fault phase [Phase 1]; $P=100 \% \pm 5 \% P_{n}$


## Test 1: 1.D.2- Asymmetrical fault phase [Phase 2]; $\mathrm{P}=100 \% \pm 5 \% \mathrm{P}_{\mathrm{n}}$



Test 1: 1.D.2- Asymmetrical fault phase [Phase 3]; $\mathbf{P}=\mathbf{1 0 0} \% \pm 5 \% \mathrm{P}_{\mathrm{n}}$


## Test 2: 2.D.2- Asymmetrical fault phase [Phase 1]; $\mathrm{P}=100 \% \pm 5 \% \mathrm{P}_{\mathrm{n}}$



Test 2: 2.D.2- Asymmetrical fault phase [Phase 2]; $\mathbf{P}=\mathbf{1 0 0} \% \pm 5 \% \mathrm{P}_{\mathrm{n}}$


## Test 2: 2.D.2- Asymmetrical fault phase [Phase 3]; $\mathrm{P}=100 \% \pm 5 \% \mathrm{P}_{\mathrm{n}}$



Test 3: 3.D.2- Asymmetrical fault phase [Phase 1]; $P=100 \% \pm 5 \% P_{n}$


## Test 3: 3.D.2- Asymmetrical fault phase [Phase 2]; $\mathrm{P}=100 \% \pm 5 \% \mathrm{P}_{\mathrm{n}}$



Test 3: 3.D.2- Asymmetrical fault phase [Phase 3]; $\mathbf{P}=\mathbf{1 0 0} \% \pm 5 \% \mathrm{P}_{\mathrm{n}}$


## Test OV1- Symmetrical fault phase; $\mathbf{P = 1 0 0 \% ~} \pm 5 \% \mathrm{P}_{\mathrm{n}}$



Test OV2- Symmetrical fault phase; $P=100 \% \pm 5 \% P_{n}$


## Test OV3- Symmetrical fault phase; $P=100 \% \pm 5 \% P_{n}$



EN 50549-1:2019: Active response to frequency deviation

| Clause | Test requirement | Test procedure according standard | Result |
| :--- | :--- | :--- | :---: |
| 4.6 .1 | Power response to over-frequency | VDE V 0124-100:2019-02 (Draft), clause <br> 5.4 .4 | $\mathbf{P}$ |
| 4.6 .2 | Power response to under-frequency | VDE V 0124-100:2019-02 (Draft), clause <br> 5.4 .6 | N/A |


| 4.6.1 Power response to over-frequency |  |  |  |  |  |  | P |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Test result: |  |  |  |  |  |  |  |
| 1-min mean value [Hz]: | a) 50,00 | b) 50,25 | c) 50,70 | d) 51,40 | e) 50,70 | f) 50,25 | g) 50,00 |
| 1. Measurement a) to g): Active power output $=100 \% P_{E_{\max }}$ $\mathrm{s}=5 \%$ ( $40 \% \mathrm{P}_{\text {ref }} / \mathrm{Hz}$ ), threshold frequency for start/return: $50,2 \mathrm{~Hz}$ |  |  |  |  |  |  |  |
| Frequency [Hz]: | 50,00 | 50,25 | 50,70 | 51,40 | 50,70 | 50,25 | 50,00 |
| PM [kW]: | N/A | 2,946 | 2,404 | 1,562 | 2,404 | 2,946 | N/A |
| $\mathrm{P}_{\text {E60 }}[\mathrm{kW}]$ : | 3,006 | 2,949 | 2,391 | 1,561 | 2,391 | 2,949 | 3,007 |
| $\Delta \mathrm{P}_{\text {E60 }} / \mathrm{P}_{\mathrm{M}}[\%]$ : | N/A | 0,11 | -0,46 | -0,06 | -0,46 | 0,12 | N/A |

## Test result:

| 1-min mean value [Hz]: | a) 50,00 | b) 50,25 | c) 50,70 | d) 51,40 | e) 50,70 | f) 50,25 | g) 50,00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

2. Measurement a) to g): Active power output $60 \%$ after freezing $=100 \% P_{\text {Emax }}$
$\mathrm{s}=5 \%\left(40 \% \mathrm{P}_{\text {ref }} / \mathrm{Hz}\right)$, threshold frequency for start/return: 50,2 Hz

| Frequency [ Hz$]$ : | 50,00 | 50,25 | 50,70 | 51,40 | 50,70 | 50,25 | 50,00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PM [kW]: | N/A | 1,736 | 1,417 | 0,922 | 1,417 | 1,736 | N/A |
| $\mathrm{P}_{\text {E60 }}[\mathrm{kW}]$ : | 1,808 | 1,771 | 1,433 | 0,942 | 1,432 | 1,772 | 3,008 |
| $\Delta \mathrm{P}_{\text {E60 }} / \mathrm{Pm}_{\text {m }}[\%]$ : | N/A | 1,18 | 0,54 | 0,65 | 0,50 | 1,21 | N/A |
| Limit $\Delta P / P_{1 \text { min }}$ : | $\pm 10 \%$ of $P_{\text {Emax }}$ |  |  |  |  |  |  |

Graph of Measurement 1.: Active power output $>80 \% P_{\text {Emax }}$


Graph of Measurement 2.:Active power output 40\% and 60\% after freezing $>80 \% \mathrm{P}_{\mathrm{n}}$


## Graph of power gradient:



## Test:

The test is conducted for two powers. First, the test must start at a power $=100 \%$ PEmax ("Measurement 1"), and in a second test, for a power 60\% PEmax ("Measurement 2"). In the second test, after freezing of the $\mathrm{P}_{\mathrm{m}}$, the available active power output must be increased to a value $=100 \% \mathrm{P}_{\text {Emax }}$, and after the network frequency of $50,2 \mathrm{~Hz}$ is fallen below, the rise of the active power gradient must be recorded.

Point g) must be held until the micro-generator is again feeding in with the active power output available.

## Assessment criterion:

For $f=50,2 \mathrm{~Hz}$, the value of the $\mathrm{P}_{\mathrm{m}}$ active power currently being generated is "frozen".
a) For adjustable micro-generators when:

1) the active power reduces between measuring points b) and f) given above with the set gradient Рм per Hz for a increasing frequency (or rises for a frequency decreasing again).
2) the maximum active power gradient occurring in point is less than the configured maximum active power per minute
3) the reaction value of the setpoint determined by the gradient characteristic curve does not differ from $P_{\text {Emax }}$ by more than $\pm 10 \%$.
4) the settling time is equal or below 2 s with an intentional delay set to zero
b) For partly adjustable micro-generators
5) when they behave as in a) within their adjustment range, and
6) when, outside the adjustable range, the power fed in on leaving the adjustment range remains constant until shutdown. Shutdown must be no later than at $51,5 \mathrm{~Hz}$.

## Note:

The test method refer to clause 5.4.4 of VDE V 0124-100:2019-02 (Draft).
The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.

EN 50549-1:2019: Power response to voltage variations and voltage changes

| Clause | Test requirement | Test procedure according standard | Result |
| :---: | :---: | :---: | :---: |
| 4.7.2.2 | Capabilities | -- | P |
| 4.7.2.3.2 | Fix control modes ( $\cos \varphi$ setpoint mode) | FGW TG3, Revision 25, clause 4.2.2 | P |
| 4.7.2.3.2 | Fix control modes (Q setpoint mode, $48,43 \%$ ) | EN 50438:2013, Annex D.3.4.2.1 | P |
| 4.7.2.2 | Q Response time | CEI 0-21:2019-04, Annex B.1.2.4 | P |
| 4.7.2.3.3 | Voltage related control modes (Q (U) controls) | VDE AR 4105:2018-05, clause 5.7.2.4. | P |
| 4.7.2.3.4 | Power related control modes $(\cos \varphi(P)$ curve) | VDE V 0124-100:2012, clause 5.3.6.4 | P |
| 4.7.3 | Voltage related active power reduction ( $\mathrm{P}(\mathrm{U})$ function) | CEI 0-21:2019-04, Annex B.1.3.1 | P |


| 4.7.2 | Voltage support by reactive power |  |
| :--- | :--- | :--- |
| 4.7.2.2 | Capabilities | P |
| 4.7.2.3.2 | Fix control modes $(\cos \varphi$ setpoint mode) |  |

## Test result:

| PF = 0,8 / Inducitive reactive power supply |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Rating power [\%] | Active power [kW] | Reactive power [kVar] | Power factor $[\cos \varphi]$ | Voltage [V] |
| 5\% | 0,148 | -0,108 | 0,8074 | 229,60 |
| 10\% | 0,284 | -0,212 | 0,8009 | 229,74 |
| 20\% | 0,589 | -0,429 | 0,8082 | 229,90 |
| 30\% | 0,890 | -0,658 | 0,8042 | 229,71 |
| 40\% | 1,193 | -0,886 | 0,8027 | 229,42 |
| 50\% | 1,491 | -1,111 | 0,8018 | 229,59 |
| 60\% | 1,790 | -1,336 | 0,8014 | 229,77 |
| 70\% | 2,087 | -1,561 | 0,8007 | 229,51 |
| 80\% | 2,382 | -1,784 | 0,8003 | 229,69 |
| 90\% | 2,403 | -1,813 | 0,7982 | 230,10 |
| 100\% | 2,398 | -1,814 | 0,7974 | 230,10 |
| PF = 0,8 / Capacitive reactive power supply |  |  |  |  |
| Rating power [\%] | Active power [kW] | Reactive power [kVar] | Power factor $[\cos \varphi]$ | Voltage [V] |
| 5\% | 0,148 | 0,114 | 0,7927 | 229,58 |
| 10\% | 0,301 | 0,231 | 0,7932 | 229,70 |
| 20\% | 0,593 | 0,456 | 0,7923 | 229,86 |
| 30\% | 0,897 | 0,682 | 0,7962 | 230,04 |
| 40\% | 1,199 | 0,907 | 0,7975 | 230,23 |
| 50\% | 1,499 | 1,132 | 0,7981 | 230,46 |
| 60\% | 1,798 | 1,355 | 0,7987 | 230,66 |
| 70\% | 2,096 | 1,576 | 0,7992 | 230,56 |
| 80\% | 2,392 | 1,796 | 0,7996 | 230,47 |
| 90\% | 2,415 | 1,823 | 0,7980 | 229,44 |
| 100\% | 2,411 | 1,822 | 0,7977 | 229,42 |


| Cos phi=1 no reactive power supply |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Rating power <br> $[\%]$ | Active power <br> $[\mathrm{kW}]$ | Reactive power <br> $[\mathrm{kVar}]$ | Power factor <br> $[\cos \varphi]$ | Voltage <br> $[\mathrm{V}]$ |  |
| $5 \%$ | 0,148 | 0,011 | 0,9971 | 229,56 |  |
| $10 \%$ | 0,288 | 0,018 | 0,9980 | 229,71 |  |
| $20 \%$ | 0,594 | 0,021 | 0,9994 | 229,45 |  |
| $30 \%$ | 0,901 | 0,020 | 0,9998 | 229,62 |  |
| $40 \%$ | 1,206 | 0,019 | 0,9999 | 229,80 |  |
| $50 \%$ | 1,509 | 0,018 | 0,9999 | 229,51 |  |
| $60 \%$ | 1,812 | 0,017 | 0,9999 | 229,69 |  |
| $70 \%$ | 2,114 | 0,016 | 0,9999 | 229,86 |  |
| $80 \%$ | 2,415 | 0,015 | 0,9999 | 229,42 |  |
| $90 \%$ | 2,711 | 0,014 | 0,9999 | 229,56 |  |
| $100 \%$ | 3,010 | 0,012 | 0,9999 | 229,74 |  |

Assessment criterion:
The power factor resulting in each of the measurement points between $20 \%$ and $90 \%$ of the nominal power is equal to or lower than 0,90 both in over excited and under excited operation.

The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.

## Diagram



| 4.7.2 | Voltage support by reactive power |  |
| :--- | :--- | :--- |
| 4.7.2.2 | Capabilities | P |
| 4.7.2.3.2 | Fix control modes (Q setpoint mode, 48,43\%) |  |

## Test result:

| Inducitive reactive power supply |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Rating power <br> $[\%]$ | Active power <br> $[\mathrm{kW}]$ | Reactive power <br> $[\mathrm{kVar}]$ | Power factor <br> $[\cos \varphi]$ | Voltage <br> $[\mathrm{V}]$ |  |
| $5 \%$ | 0,156 | $-1,816$ | 0,0859 | 229,63 |  |
| $10 \%$ | 0,293 | $-1,807$ | 0,1598 | 229,70 |  |
| $20 \%$ | 0,556 | $-1,832$ | 0,2904 | 229,44 |  |
| $30 \%$ | 0,863 | $-1,830$ | 0,4265 | 229,63 |  |
| $40 \%$ | 1,171 | $-1,830$ | 0,5389 | 229,21 |  |
| $50 \%$ | 1,478 | $-1,811$ | 0,6320 | 229,39 |  |
| $60 \%$ | 1,780 | $-1,812$ | 0,7007 | 230,02 |  |
| $70 \%$ | 2,083 | $-1,812$ | 0,7544 | 230,21 |  |
| $80 \%$ | 2,384 | $-1,812$ | 0,7961 | 230,39 |  |
| $90 \%$ | 2,403 | $-1,815$ | 0,7979 | 230,41 |  |
| $100 \%$ | 2,397 | $-1,815$ | 0,7971 | 230,35 |  |


| Capacitive reactive power supply |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Rating power <br> $[\%]$ | Active power <br> $[\mathrm{kW}]$ | Reactive power <br> $[\mathrm{kVar}]$ | Power factor <br> $[\cos \varphi]$ | Voltage <br> $[\mathrm{V}]$ |  |
| $5 \%$ | 0,154 | 1,818 | 0,0841 | 229,16 |  |
| $10 \%$ | 0,298 | 1,827 | 0,1607 | 229,09 |  |
| $20 \%$ | 0,586 | 1,820 | 0,3072 | 229,48 |  |
| $30 \%$ | 0,869 | 1,821 | 0,4303 | 229,72 |  |
| $40 \%$ | 1,176 | 1,819 | 0,5429 | 230,05 |  |
| $50 \%$ | 1,481 | 1,831 | 0,6289 | 230,42 |  |
| $60 \%$ | 1,786 | 1,831 | 0,6982 | 230,61 |  |
| $70 \%$ | 2,093 | 1,828 | 0,7531 | 230,14 |  |
| $80 \%$ | 2,389 | 1,829 | 0,7940 | 230,97 |  |
| $90 \%$ | 2,415 | 1,823 | 0,7980 | 230,99 |  |
| $100 \%$ | 2,410 | 1,823 | 0,7975 | 230,99 |  |


| Cos phi=1 no reactive power supply |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Rating power <br> $[\%]$ | Active power <br> $[\mathrm{kW}]$ | Reactive power <br> $[\mathrm{kVar}]$ | Power factor <br> $[\cos \varphi]$ | Voltage <br> $[\mathrm{V}]$ |
| $5 \%$ | 0,148 | 0,011 | 0,9971 | 229,56 |
| $10 \%$ | 0,288 | 0,018 | 0,9980 | 229,71 |
| $20 \%$ | 0,594 | 0,021 | 0,9994 | 229,45 |
| $30 \%$ | 0,901 | 0,020 | 0,9998 | 229,62 |
| $40 \%$ | 1,206 | 0,019 | 0,9999 | 229,80 |
| $50 \%$ | 1,509 | 0,018 | 0,9999 | 229,51 |
| $60 \%$ | 1,812 | 0,017 | 0,9999 | 229,69 |
| $70 \%$ | 2,114 | 0,016 | 0,9999 | 229,86 |
| $80 \%$ | 2,415 | 0,015 | 0,9999 | 229,42 |
| $90 \%$ | 2,711 | 0,014 | 0,9999 | 229,56 |
| $100 \%$ | 3,010 | 0,012 | 0,9999 | 229,74 |

## Assessment criterion:

The power factor resulting in each of the measurement points between $20 \%$ and $90 \%$ of the nominal power is equal to or lower than 0,90 both in over excited and under excited operation,

The test method refer to clause CEI0-21 / EN 50438:2013, Annex D, 3, 4,2,1,
Generating plants must meet the reactive power requirement regardless of the number of feeding phases under normal steady-state operating conditions in the voltage tolerance band $+10 \% U_{n}$ and $-15 \% U_{n}$.

The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.

## Diagram



| 4.7.2.2 | Capabilities <br> Q Response time |  | P |
| :---: | :---: | :---: | :---: |
| Reaction time |  |  |  |
| Test result: |  |  |  |
|  |  | Time | Result |
| 1. | Reaction time Q=0 to Qmin (50\% test) | 3,2s | P |
| 2. | Reaction time Qmin to Qmax ( $50 \%$ test) | 7,6 s | P |
| 3. | Reaction time Qmax to Q=0 ( $50 \%$ test) | 4,0 s | P |
| 4. | Reaction time Q=0 to Qmin ( $100 \%$ test) | 5,4 s | P |
| 5. | Reaction time Qmin to Qmax (100\% test) | 8,4 s | P |
| 6. | Reaction time Qmax to Q=0 (100\% test) | 4,0 s | P |

Test result:
Graph 50\%Pn



## Assessment criterion:

DC source should be set to $50 \%$ (test1) and $100 \%$ (test2) output power micro-generator.
Starting with $Q=0$ then $Q \min \leq-0,4843$ Pn to to $Q \max \geq 0,4843$ Pn, and then back to $Q=0$ in doing so each point must be kept for at least 2 minute.

The total tolerance is $\Delta \mathrm{Q} \leq \pm 5,0 \%$ of Pn or $\Delta \cos \varphi \leq \pm 0,01$
The maximum response time is 10 s .
The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.

### 4.7.2.2 Capabilities

### 4.7.2.3.3 Voltage related control modes (Q (U) controls)

The validation of the $Q(U)$ regulation according to VDE-AR-N 4105: 2018-05, 5.7.2.4 is divided into two partial tests, so that on the one hand the accuracy and on the other hand the dynamics of the $Q(U)$ control is checked. For all inverter-coupled systems, only the inverter must be tested.

## Test result:

Test of the reactive power-voltage characteristic $Q(U)$

| $\operatorname{Vac}\left[\% \mathrm{U}_{\mathrm{n}}\right.$ ] <br> Set point | Vac_L1 [V] measured | P [kW] <br> measured | Q [kVar] measured | Q [kVar] expected | $\begin{gathered} \Delta \mathrm{Q} \\ {\left[\% \mathrm{P}_{\mathrm{Emax}}\right]} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 100 | 230,12 | 3,004 | 0,013 | 0,000 | 0,426 |
| 99 | 227,75 | 3,003 | 0,012 | 0,000 | 0,389 |
| 98 | 225,69 | 3,002 | 0,010 | 0,000 | 0,348 |
| 97 | 223,18 | 3,001 | 0,011 | 0,000 | 0,373 |
| 96 | 220,60 | 2,999 | 0,433 | 0,450 | -0,568 |
| 95 | 218,44 | 2,890 | 0,865 | 0,900 | -1,173 |
| 94 | 216,01 | 2,681 | 1,342 | 1,350 | -0,261 |
| 93 | 213,74 | 2,382 | 1,797 | 1,800 | -0,112 |
| 92 | 211,47 | 2,326 | 1,821 | 1,800 | 0,684 |
| 91 | 209,39 | 2,289 | 1,823 | 1,800 | 0,770 |
| 90 | 207,07 | 2,249 | 1,822 | 1,800 | 0,730 |
| 91 | 209,38 | 2,288 | 1,823 | 1,800 | 0,774 |
| 92 | 211,63 | 2,329 | 1,821 | 1,800 | 0,691 |
| 93 | 213,74 | 2,383 | 1,796 | 1,800 | -0,133 |
| 94 | 216,00 | 2,682 | 1,340 | 1,350 | -0,333 |
| 95 | 218,36 | 2,887 | 0,875 | 0,900 | -0,828 |
| 96 | 220,59 | 2,999 | 0,433 | 0,450 | -0,579 |
| 97 | 223,17 | 3,001 | 0,011 | 0,000 | 0,381 |
| 98 | 225,69 | 3,002 | 0,010 | 0,000 | 0,348 |
| 99 | 227,76 | 3,005 | 0,011 | 0,000 | 0,377 |
| 100 | 230,14 | 3,004 | 0,014 | 0,000 | 0,458 |
| 101 | 232,26 | 3,008 | 0,013 | 0,000 | 0,439 |
| 102 | 234,63 | 3,009 | 0,012 | 0,000 | 0,414 |
| 103 | 236,92 | 3,010 | -0,044 | 0,000 | -1,479 |
| 104 | 238,99 | 3,001 | -0,453 | -0,450 | -0,095 |
| 105 | 241,33 | 2,882 | -0,914 | -0,900 | -0,454 |
| 106 | 243,60 | 2,690 | -1,364 | -1,350 | -0,453 |
| 107 | 246,11 | 2,407 | -1,809 | -1,800 | -0,315 |
| 108 | 248,34 | 2,408 | -1,809 | -1,800 | -0,309 |


| 109 | 250,72 | 2,410 | $-1,809$ | $-1,800$ | $-0,290$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 110 | 253,10 | 2,411 | $-1,809$ | $-1,800$ | $-0,289$ |
| 109 | 250,73 | 2,409 | $-1,808$ | $-1,800$ | $-0,282$ |
| 108 | 248,36 | 2,408 | $-1,809$ | $-1,800$ | $-0,289$ |
| 107 | 246,13 | 2,407 | $-1,810$ | $-1,800$ | $-0,319$ |
| 106 | 243,62 | 2,689 | $-1,365$ | $-1,350$ | $-0,511$ |
| 105 | 241,35 | 2,879 | $-0,922$ | $-0,900$ | $-0,736$ |
| 104 | 239,01 | 3,000 | $-0,455$ | $-0,450$ | $-0,172$ |
| 103 | 236,94 | 3,010 | $-0,057$ | 0,000 | $-1,891$ |
| 102 | 234,64 | 3,009 | 0,014 | 0,000 | 0,464 |
| 101 | 232,27 | 3,007 | 0,013 | 0,000 | 0,423 |
| 100 | 230,20 | 3,006 | 0,013 | 0,000 | 0,433 |
| Limit $\Delta \mathbf{Q}:$ |  | $\pm 4 \% \mathrm{P}_{\mathrm{Emax}}$ |  |  |  |

## Graph of characteristic $\mathbf{Q}(\mathrm{U})$ :



## Test:

The verification of the accuracy of the $Q(U)$ control of the reactive power-voltage characteristic Un shown in VDE-AR-N 4105: 2018-11, 5.7.2.4, Figure 7 is effected by a slow variation of the line voltage $U_{n}$ in the range $90 \% U_{n}$ to $110 \% U_{n}$. Depending on the type of EZE (single- or three-phase), the voltage changes must be carried out simultaneously or symmetrically on all phases.
a) In order to check the stationary accuracy, the permissible voltage range shall be passed through within steps, with a step size of $1 \% U_{n}$, but not greater than $2 \% U_{n}$.

1. Pass the voltage range from $100 \% U_{n}$ down to the under voltage range to $90 \% U_{n}$.
2. Pass the voltage range from $90 \% U_{n}$ up to the over voltage range to $110 \% U_{n}$.
3. Pass the voltage range from $110 \% U_{n}$ down to the Nominal Voltage $U_{n}$.

The procedure is analogous to Figure 3 in Section 5.4.3.2.


The voltages are to be set with a maximum deviation of $0.25 \% U_{n}$.

## Assessment criterion:

In order to pass the $Q(U)$ accuracy test, the measured stationary value pairs UPGU and Qpgu, under taking account to the correct sign in the consumer metering system, must be within VDE-AR-N 4105: 2018-11, in 5.7.2.4, Figure 7 Q (U) shown characteristic. The stationary value pairs UpGu and Qpgu are determined by averaging over 30 seconds at the end of the respective measuring section analogously to Chapter 5.4.3.2. The permissible deviations are with the maximum measuring error of the voltage of $1 \% U_{n}$ stated in VDE-ARN 4105: 2018-11 and a setting accuracy of 4\% P PMax at

$$
Q_{E Z E, t o l}= \pm\left(0.01 \cdot \mathrm{U}_{\mathrm{N}, \mathrm{Y}} \cdot \mathrm{k}_{\mathrm{QU}}+0.04 \cdot P_{E M a x}\right)= \pm 0,25 \cdot P_{E M a x} \cdot\left(\sin \left(\arccos \left(\varphi_{\min }\right)\right)+0.16\right)
$$

The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.

| Test of the dynamics of the Q (U) regulation |  | P |  |
| :---: | :---: | :---: | :---: | :---: |
| Voltage jump Vac [\% $U_{n}$ ] | Q [kVar] measured | Q [\%Qmax] measured | T=3Tmeasured |
|  | $-1,536$ | $-85,35$ | $6,6 \mathrm{~s}$ |
|  | $-1,536$ | $-85,35$ | $6,8 \mathrm{~s}$ |
|  | $-1,538$ | $-85,42$ | $6,6 \mathrm{~s}$ |
| 100 to 93,6 | 1,519 | 84,37 | $7,8 \mathrm{~s}$ |
|  | 1,520 | 84,45 | $7,8 \mathrm{~s}$ |

## Note:

The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.

## Graph of $100 \% U_{n}$ to $\mathbf{1 0 6 , 4 \%} U_{n}$ : Test 1



Graph of $\mathbf{1 0 0 \%} \mathrm{U}_{\mathrm{n}}$ to $\mathbf{1 0 6 , 4 \%} \mathrm{U}_{\mathrm{n}}$ : Test 2


## Graph of $\mathbf{1 0 0 \%} \mathrm{U}_{\mathrm{n}}$ to $\mathbf{1 0 6 , 4 \%} \mathrm{U}_{\mathrm{n}}$ : Test 3



Graph of $100 \% \mathrm{U}_{\mathrm{n}}$ to $93,6 \% \mathrm{U}_{\mathrm{n}}$ : Test 1


## Graph of $100 \% U_{n}$ to $93,6 \% U_{n}$ : Test 2



Graph of $100 \% U_{n}$ to $93,6 \% U_{n}$ : Test 3


| 4.7.2.2 Capabilities <br> 4.7.2.3.4 Power related Control mode $(\cos \varphi(P)$ curve) |  |  |  |  |  |  |  |  |  | P |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Test result: |  |  |  |  |  |  |  |  |  |  |
| Test a): |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{P}_{\text {Emax }} / \mathrm{P}$ [\%] | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 |
| 30 s mean value | 20\% to 100\% P $\mathrm{Emax}^{\text {max }}$ |  |  |  |  |  |  |  |  |  |
| U [V]: | N/A | 229,52 | 229,71 | 229,90 | 230,10 | 230,31 | 230,49 | 230,69 | 230,88 | 230,88 |
| $\mathrm{P}_{\mathrm{E} 30}[\mathrm{~kW}]$ : | N/A | 0,594 | 0,900 | 1,205 | 1,508 | 1,833 | 2,109 | 2,405 | 2,702 | 2,762 |
| $\mathrm{P}_{\text {E30 }}$ of $\mathrm{P}_{\text {Emax }}$ [\%]: | N/A | 19,80 | 30,00 | 40,17 | 50,27 | 61,10 | 70,28 | 80,17 | 90,06 | 92,08 |
| QE30 [kVAr]: | N/A | 0,021 | 0,020 | 0,019 | 0,018 | -0,356 | -0,593 | -0,850 | -1,125 | -1,203 |
| $\cos \varphi_{\text {Езо }}$ : | N/A | 0,9994 | 0,9997 | 0,9999 | 0,9999 | 0,9814 | 0,9627 | 0,9429 | 0,9231 | 0,9168 |
| $\cos \varphi_{\text {setpoint }}$ of $\mathrm{P}_{\text {E } 30}$ : | N/A | 1,000 | 1,000 | 1,000 | 1,000 | 0,980 | 0,960 | 0,940 | 0,920 | 0,920 |
| Limit $\cos \varphi_{\text {e }}$ \% |  |  |  |  | $\cos \varphi_{\text {setpo }}$ | int $\pm 0,01$ |  |  |  |  |
| Test b): |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{P}_{\text {Emax }} / \mathrm{P}_{\mathrm{n}}$ [\%] |  | 20 |  |  | 5 | 0 |  |  | 100 |  |
| 30 s mean value | 20\% to $50 \%$ to $100 \% \mathrm{P}_{\mathrm{Emax}}$ |  |  |  |  |  |  |  |  |  |
| U [V]: | 230,32 |  |  | 230,88 |  |  |  | 231,54 |  |  |
| $\mathrm{P}_{\text {E30 }}$ [kW]: | 0,599 |  |  | 1,512 |  |  |  | 2,763 |  |  |
| $\mathrm{P}_{\text {E }}$ 0 of $\mathrm{P}_{\text {Emax }}$ [\%]: | 19,97 |  |  | 50,42 |  |  |  | 92,09 |  |  |
| Q Eзо [kVAr]: $^{\text {a }}$ | 0,022 |  |  | 0,019 |  |  |  | -1,203 |  |  |
| $\cos \varphi_{\text {Е }}$ \% | 0,9993 |  |  | 0,9999 |  |  |  | 0,9168 |  |  |
| $\cos \varphi_{\text {setpoint }}$ of $\mathrm{P}_{\text {E } 30}$ : | 1,000 |  |  | 1,000 |  |  |  | 0,920 |  |  |
| To[s]: | <1,0s |  |  |  |  | 4,4s |  |  |  |  |
| $\mathrm{P}_{\text {Emax }} / \mathrm{P}_{\mathrm{n}}$ [\%] | 100 |  |  | 50 |  |  |  | 20 |  |  |
| 30 s mean value | 100\% to $50 \%$ to $20 \% \mathrm{P}_{\mathrm{Emax}}$ |  |  |  |  |  |  |  |  |  |
| U [V]: | 231,09 |  |  | 230,29 |  |  |  | 229,74 |  |  |
| P езо $^{\text {[kW] }}$ : | 2,762 |  |  | 1,511 |  |  |  | 0,598 |  |  |
| $\mathrm{P}_{\text {езо }}$ [\%]: | 92,08 |  |  | 50,35 |  |  |  | 19,94 |  |  |
| Q E30 [kVAr]: $^{\text {a }}$ | -1,204 |  |  | 0,018 |  |  |  | 0,021 |  |  |
| $\cos \varphi_{\text {Е } 30}$ : | 0,9167 |  |  | 0,9999 |  |  |  | 0,9994 |  |  |
| $\cos \varphi_{\text {setpoint }}$ of $\mathrm{P}_{\text {ез }}$ : | 0,920 |  |  | 1,000 |  |  |  | 1,000 |  |  |
| To [s]: | 5,4s |  |  |  |  | <1,0s |  |  |  |  |
| Limit $\mathrm{T}_{0}$ [s]: | 10 s |  |  |  |  |  |  |  |  |  |
| Limit $\cos \varphi_{\text {e } 30}$ : | $\cos \varphi_{\text {setpoint }} \pm 0,02$ |  |  |  |  |  |  |  |  |  |



Graph of setting ( $\mathrm{T}_{0}$ ) time: Test b): $\mathbf{2 0 \%}$ to $\mathbf{5 0 \%}$ to $\mathbf{1 0 0 \%}$ to $\mathbf{5 0 \%}$ to $\mathbf{2 0 \%}$


## Test:

Test 1: Using the standard characteristic curve increases the active power from $20 \%$ PEmax in increments of $10 \% \mathrm{Pemax}$ to $\mathrm{P}_{\text {Emax }}$, The test is carried out in reverse.
Test 2: Using the standard characteristic curve increases the active power from $20 \% \mathrm{P}_{\text {Emax }}$ to $50 \% \mathrm{P}_{\text {Emax }}$ and to $P_{\text {Emax, }}$, The test is carried out in reverse, After the PGU has settled, the end value reached is determined as a 30 s mean value.

*) Depending on $S_{\text {Amax }}$.

## Assessment criterion:

Test 1: $\cos \varphi$ accuracy $\cos \varphi( \pm 0,01)$
Test 2: $\cos \varphi$ accuracy $\cos \varphi( \pm 0,02)$
For the test to be passed, the $\cos \varphi$ setpoint from the active power must be measured at the terminals of the PGU within a settling time of 10 s .

## Note:

The test method refer to clause 5,3,6,4 of VDE V 0124-100:2012-07.
The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.

| 4.7.3 Voltage related active power reduction (P(U) function) |  | P |
| :---: | :---: | :---: |
| Test result: |  |  |
| Test: |  |  |
| 5-min mean value / $P /$ $P_{n}[\%]$ | 100\% to 20\% |  |
| Settling time [s]: | $6 s$ |  |
| $\mathrm{P}_{\text {E60 }}$ [\%]: | 19,7 |  |
| $\Delta \mathrm{P}_{\text {E60 }} / \mathrm{P}_{\text {Setpoint }}[\%]$ \% | 20 \% or less of $P$ |  |
| Limit settling time: | 600s |  |

Test:
a) Set the voltage to $2 \% \mathrm{Vn}$ lower than the activation threshold stated by the manufacturer.
b) Set the voltage to $112 \% \mathrm{Vn}$, The inverter now has to reduce its output power to value lower than $20 \% \mathrm{Pn}$ within 5 min .
c) Set the voltage back to $2 \% \mathrm{Vn}$ lower than the activation threshold, Check that the active power will return to the value consistent with the power available from the primary source or simulated.
The test had been performed on the model ASW1000S-S, the test results are valid for the ASW3000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.

## Assessment criterion:

for adjustable PGUs:

- no network disconnection
- the active power value does not exceed the setpoint of $20 \% \mathrm{P}_{\text {Emax }}$
- the setting time determind is equal or less than 600s



## EN 50549-1:2019: Power quality

| Clause | Test requirement | Test procedure according standard | Result |
| :--- | :--- | :--- | :---: |
| 4,8 | EMC and power quality | -- | P |
|  | Harmonic current emission | EN 61000-3-2, <br> EN 61000-3-12 | P |
|  | Harmonic current emission | EN 61000-4-7 | N/A |
|  | Switching operations | IEC 61400-21 | P |
|  | Voltage fluctuation and flicker | EN 61000-3-3, <br> EN 61000-3-11 | P |
|  | Flicker and voltage fluctuations | IEC 61400-21 | P |
|  | DC injection | EN 50438, Annex D,3,10 | P |
|  | Immunity to voltage dips and short <br> interruptions | G59/3-4:2018-05, clause 13.8.4.5 | P |
|  | Unbalance | BDEW TG3, Revision 25, clause 4.3.5 | N/A |


| 4.8 | EMC and power quality <br> Harmonic current emission (EN 61000-3-2) |  |  | P |
| :---: | :---: | :---: | :---: | :---: |
| Test result: |  |  |  |  |
| Watts [kW] |  | 3,005 |  |  |
| Vrms [V] |  |  | 230,34 |  |
| Arms [A] |  | 13,057 |  |  |
| Frequency [ Hz ] |  | 50,000 |  |  |
| THD40* (100\% output power) |  |  | 2,098 |  |
| Harmonic order n | Current Magnitude [A] at $100 \%$ rated output power | \% of Fundamental | Phase | Harmonic Current Limits [A] |
| 1st | 13,023 | 100,000 | Single-phase | - |
| 2nd | 0,074 | 0,722 | Single-phase | 1,080 |
| 3rd | 0,078 | 0,660 | Single-phase | 2,300 |
| 4th | 0,016 | 0,161 | Single-phase | 0,430 |
| 5th | 0,072 | 0,579 | Single-phase | 1,140 |
| 6th | 0,010 | 0,104 | Single-phase | 0,300 |
| 7th | 0,017 | 0,154 | Single-phase | 0,770 |
| 8th | 0,008 | 0,082 | Single-phase | 0,230 |
| 9th | 0,083 | 0,652 | Single-phase | 0,400 |
| 10th | 0,008 | 0,074 | Single-phase | 0,184 |
| 11th | 0,070 | 0,551 | Single-phase | 0,330 |
| 12th | 0,008 | 0,070 | Single-phase | 0,153 |
| 13th | 0,055 | 0,433 | Single-phase | 0,210 |
| 14th | 0,007 | 0,066 | Single-phase | 0,131 |
| 15th | 0,043 | 0,337 | Single-phase | 0,150 |
| 16th | 0,007 | 0,062 | Single-phase | 0,115 |
| 17th | 0,028 | 0,219 | Single-phase | 0,132 |
| 18th | 0,007 | 0,059 | Single-phase | 0,102 |
| 19th | 0,018 | 0,143 | Single-phase | 0,118 |
| 20th | 0,007 | 0,060 | Single-phase | 0,092 |
| 21th | 0,013 | 0,110 | Single-phase | 0,107 |
| 22th | 0,009 | 0,079 | Single-phase | 0,084 |
| 23th | 0,015 | 0,119 | Single-phase | 0,098 |
| 24th | 0,009 | 0,071 | Single-phase | 0,077 |
| 25th | 0,010 | 0,086 | Single-phase | 0,090 |
| 26th | 0,007 | 0,057 | Single-phase | 0,071 |
| 27th | 0,009 | 0,077 | Single-phase | 0,083 |
| 28th | 0,006 | 0,053 | Single-phase | 0,066 |
| 29th | 0,010 | 0,078 | Single-phase | 0,078 |
| 30th | 0,007 | 0,055 | Single-phase | 0,061 |
| 31th | 0,009 | 0,076 | Single-phase | 0,073 |
| 32th | 0,007 | 0,058 | Single-phase | 0,058 |
| 33th | 0,009 | 0,075 | Single-phase | 0,680 |
| 34th | 0,007 | 0,057 | Single-phase | 0,054 |
| 35th | 0,009 | 0,072 | Single-phase | 0,064 |
| 36th | 0,008 | 0,065 | Single-phase | 0,051 |
| 37th | 0,011 | 0,086 | Single-phase | 0,061 |
| 38th | 0,010 | 0,082 | Single-phase | 0,048 |
| 39th | 0,013 | 0,103 | Single-phase | 0,058 |
| 40th | 0,008 | 0,064 | Single-phase | 0,046 |

## Note:

The tests should be based on the limits of the EN61000-3-2 for less than 16A and on EN 61000-3-12 for more than 16A.
The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.

| $4.8 \quad$ EMC and power quality Switching operation (Refer IEC 61400-21) |  |  |  | P |
| :---: | :---: | :---: | :---: | :---: |
| Test result: |  |  |  |  |
| Max. number of switching operations, $\mathrm{N}_{10}$ | 10 |  |  |  |
| Max. number of switching operations, $\mathrm{N}_{120}$ | 120 |  |  |  |
| Case of switching operation | Cut-in at $9 \% \mathrm{P}_{\text {Emax }}$ |  |  |  |
| Grid impedance angle, $\Psi_{\mathrm{k}}$ | $30^{\circ}$ | $50^{\circ}$ | $70^{\circ}$ | $85^{\circ}$ |
| Flicker step factor, $\mathrm{k}_{\mathrm{f}}\left(\Psi_{\mathrm{k}}\right)$ | 0,061 | 0,039 | 0,032 | 0,030 |
| Voltage change factor, $\left.\mathrm{ku}^{( } \Psi_{\mathrm{k}}\right)$ | 1,519 | 1,553 | 1,581 | 1,505 |
| Maximum inrush current factor kimax | 0,074 |  |  |  |
| Case of switching operation | Cut-in at $100 \% \mathrm{P}_{\text {Emax }}$ |  |  |  |
| Grid impedance angle, $\psi_{\mathrm{k}}$ | $30^{\circ}$ | $50^{\circ}$ | $70^{\circ}$ | $85^{\circ}$ |
| Flicker step factor, $\mathrm{k}_{\mathrm{f}}\left(\psi_{\mathrm{k}}\right)$ | 0,341 | 0,222 | 0,181 | 0,170 |
| Voltage change factor, $\left.\mathrm{ku}^{( } \Psi_{\mathrm{k}}\right)$ | 4,125 | 4,087 | 4,163 | 4,111 |
| Maximum inrush current factor kimax | 0,571 |  |  |  |
| Case of switching operation | Service disconnection at rated power |  |  |  |
| Grid impedance angle, $\Psi_{\mathrm{k}}$ | $30^{\circ}$ | $50^{\circ}$ | $70^{\circ}$ | $85^{\circ}$ |
| Flicker step factor, $\mathrm{k}_{\mathrm{f}}\left(\Psi_{\mathrm{k}}\right)$ | 0,685 | 0,443 | 0,359 | 0,339 |
| Voltage change factor, $\left.\mathrm{ku}^{( } \Psi_{\mathrm{k}}\right)$ | 4,353 | 4,511 | 4,411 | 4,334 |
| Maximum inrush current factor kimax | 0,569 |  |  |  |
| Worst case over all switching operations, $\mathrm{k}_{\text {imax }}$ | 0,571 |  |  |  |
| Note: <br> $S_{k, \text { fic }} / S_{n}$ in the fictitious grid was set to: 63. <br> The test had been performed on the model ASW1000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software. |  |  |  |  |

## Diagram of measured voltage, current, apparent active and reactive power at cut in at $9 \% \mathrm{P}_{\text {Emax }}$



Diagram of measured voltage, current, apparent active and reactive power at cut in at $100 \% \mathrm{P}_{\text {Emax }}$


Diagram of measured voltage, current, apparent active and reactive power at service disconnection



## Note:

*The stationary deviance of dc\% is more relevant than the dynamic deviance of dmax at starting and stopping, Mains Impedance according EN61000-3-11:
$R \max =0,24 \Omega$; jXmax $=0,15 \Omega @ 50 H z(|Z \max |=0,283 / 0,4717 \Omega$ ) for single phase inverter use also $R_{n}=0,16 \Omega ; j X_{n}=0,1 \Omega$.
Calculation of the maximum permissible grid impedance at the point of common coupling based on dc:
$\mathbf{Z}_{\text {max }}=\mathbf{Z}_{\text {ref }}{ }^{*} \mathbf{3 , 3 \%} / \mathbf{d}_{\mathrm{c}}\left(\mathbf{P}_{\mathrm{n}}\right)$.
The tests should be based on the limits of the EN 61000-3-3 for less than 16A and on EN 61000-3-11 for more than 16A.

The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.

| $\begin{array}{ll}\text { 4.8 } & \begin{array}{l}\text { EMC and power quality } \\ \text { Flicker and voltage fluctuations }\end{array} \\ & \end{array}$ |  |  |  |  |  |  |  |  |  | P |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Method: Measurement and evaluation was carried out according to the procedure in IEC 61400-21. |  |  |  |  |  |  |  |  |  |  |
| Test result: |  |  |  |  |  |  |  |  |  |  |
| Grid impedance angle, $\Psi_{\mathrm{k}}$ |  |  | $30^{\circ}$ |  | $50^{\circ}$ |  | $70^{\circ}$ |  |  |  |
| Operating point, $\mathrm{Pa}_{\mathrm{a}} \mathrm{P}_{\text {Emax }}[\%]$ |  |  | Flicker coefficient, $\mathrm{c}\left(\Psi_{\mathrm{k}}\right)$ |  |  |  |  |  |  |  |
| 0 |  |  | 4,290 | 2,800 |  |  | 2,283 |  | 2,153 |  |
| 10 |  |  | 4,290 | 2,800 |  |  | 2,283 |  | 2,153 |  |
| 20 |  |  | 4,290 | 2,800 |  |  | 2,283 |  | 2,153 |  |
| 30 |  |  | 4,290 | 2,800 |  |  | 2,283 |  | 2,153 |  |
| 40 |  |  | 4,290 | 2,800 |  |  | 2,283 |  | 2,153 |  |
| 50 |  |  | 4,290 | 2,800 |  |  | 2,283 |  | 2,153 |  |
| 60 |  |  | 4,290 | 2,800 |  |  | 2,283 |  | 2,153 |  |
| 70 |  |  | 4,290 | 2,800 |  |  | 2,283 |  | 2,153 |  |
| 80 |  |  | 4,290 | 2,800 |  |  | 2,283 |  | 2,153 |  |
| 90 |  |  | 4,290 | 2,800 |  |  | 2,283 |  | 2,153 |  |
| 100 |  |  | 4,290 | 2,800 |  |  | 2,283 |  | 2,153 |  |
| Max. Flicker coefficient, $\mathrm{c}(\psi \mathrm{k})$ |  |  | 4,290 | 2,800 |  |  | 2,283 |  | 2,153 |  |
| Max. Short-term flicker, Pst |  |  | 0,068 | 0,044 |  |  | 0,036 |  | 0,034 |  |
|  |  |  |  |  |  |  |  |  |  |  |
| Reactive power setpoint during testing [kVar] |  |  |  | 0 |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
| P [\%PEmax] | 0 | 10 | 20 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 |
| Number of data sets | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
|  |  |  |  |  |  |  |  |  |  |  |
| Note: |  |  |  |  |  |  |  |  |  |  |
| The table entries are worst case values. |  |  |  |  |  |  |  |  |  |  |
| $S_{k, \text { fic }} / S_{n}$ in the fictitious grid was set to: 63. |  |  |  |  |  |  |  |  |  |  |
| The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software. |  |  |  |  |  |  |  |  |  |  |

## Maximum Flicker coefficients $\mathrm{c}\left(\Psi_{\mathrm{k}}\right)$ vs. power bins




## Note:

Test method and setting value refer Annex D.3.10 of EN 50438:2013.
Testing must be performed according to WI 10.4.-03.doc rev D. The internal temperature of the EUT must be stabilized, No temperature drift of more than 2K within 1 hour is allowed.
The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.


| 4，8 Immunity to voltage dips and short interruptions |  |  |  |  | P |
| :---: | :---: | :---: | :---: | :---: | :---: |
| For a directly coupled SSEG |  |  | For a Inverter SSEG |  |  |
| Parameter | Symbol | Value | Time after fault | Volts | Amps |
| Peak Short Circuit current | $1 p$ | N／A | 20 ms | 29，80 | 3，393 |
| Initial Value of aperiodic current | A | N／A | 100ms | 30，10 | 4，094 |
| Initial symmetrical short－circuit current＊ | $l_{k}$ | N／A | 250ms | 30，59 | 7，819 |
| Decaying（aperiodic） component of short circuit current＊ | idc | N／A | 500ms | N／A | N／A |
| Reactance／Resistance Ratio of source＊ | X／R | N／A | Time to trip | 0，522 | In second |
| Diagram |  |  |  |  |  |
|  |  |  | Wununuwnuy | WWMWM |  |
| Note： <br> For rotating machines and linea current as seen at the Generating <br> ＊Values for these parameters s interpolation of the plot． <br> The test had been performed on ASW1500S－S，ASW2000S－S si | iston ma Unit term uld be provic <br> he model it is iden | ines the als． <br> ided wh <br> SW3000 <br> cal in ha | st should produc <br> the short circuit <br> S，the test result ware and softwa | $0 s-2 s \text { plo }$ <br> ation is <br> valid for | hort circuit ong to ena 1000S-S, |

EN 50549-1:2019: Interface protection

| Clause | Test requirement | Test procedure according standard | Result |
| :--- | :--- | :--- | :---: |
| 4.9 .3 | Requirements on voltage and frequency <br> protection | CEI 0-21:2019-04, Annex A.3.1 to A.3.4 | P |
| $4,9,3,1$ | Undervoltage protection | EN 50438, Annex D.2.3 | P |
|  | Overvoltage protection | EN 50438, Annex D.2.3 | P |
|  | Overvoltage 10 min mean protection | EN 50160 | $\mathbf{P}$ |
|  | Underfrequency protection | EN 50438, Annex D.2.4 | $\mathbf{P}$ |
|  | Overfrequency protection | EN 50438, Annex D.2.4 | $\mathbf{P}$ |
| 4.9 .4 .2 | Loss of Mains (LoM) detection | IEC 62116:2014 | $\mathbf{P}$ |


| 4.9.3 | Requirements on voltage and frequency protection Checklist |  |  |  |  |  |  |  | P |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Several points to check |  |  |  |  |  |  |  |  |  |
| Clause 4.9.3.1 to 4.9.3.6 | All thresholds must be adjustable |  |  |  |  |  |  |  | P |
| Voltage values |  |  |  |  |  |  |  |  |  |
| Threshold | Stage 1 [27 <] |  |  |  | Stage 2 [27 <<] |  |  |  |  |
|  | Operate voltage |  | Operate time |  | Operate voltage |  | Operate time |  |  |
| Range | 0,2-1,0 Un |  | 0,1-100s |  | 0,2-1,0 Un |  | 0,1-5s |  |  |
| Steps | 0,01 Un |  | 0,1 s |  | 0,01 Un |  | 0,05s |  |  |
| Threshold | Stage 1 [59 >] |  |  | Stage 2 [59 >>] |  | Overvoltage 10 min mean protection |  |  |  |
|  | Operate voltage | Operate time |  | Operate voltage | Operate time | Operate voltage |  | Operate time |  |
| Range | 1,0-1,2 $\mathrm{U}_{\mathrm{n}}$ | 0,1-100s |  | 1,0-1,3 $\mathrm{U}_{\mathrm{n}}$ | 0,1-5s | 1,0-1,15 Un |  | 3s not adjustable |  |
| Steps | $0,01 U_{n}$ | 0,1s |  | 0,01 Un | 0,05s | $0,01 U_{n}$ |  |  |  |
| Frequency values |  |  |  |  |  |  |  |  |  |
| Threshold | Stage 1 [81 <] |  |  |  | Stage 2 [81<<] |  |  |  |  |
|  | Operate frequency |  | Operate time |  | Operate frequency |  | Operate time |  |  |
| Range | $47,0-50,0 \mathrm{~Hz}$ |  | 0,1-100s |  | 47,0-50,0Hz |  | 0,1-5s |  |  |
| Steps | $0,1 \mathrm{~Hz}$ |  |  | ,1 s | $0,1 \mathrm{~Hz}$ |  | 0,05s |  |  |
| Threshold | Stage 1 [81 >] |  |  |  | Stage 2 [81 >>] |  |  |  |  |
|  | Operate frequency |  | Operate time |  | Operate frequency |  | Operate time |  |  |
| Range | $50,0-52,0 \mathrm{~Hz}$ |  |  | -100s | 50,0-52,0Hz |  | 0,1-5s |  |  |
| Steps | $0,1 \mathrm{~Hz}$ |  |  | , s | $0,1 \mathrm{~Hz}$ |  | 0,05s |  |  |
| 4.9.2.6 | Insensitive against 40ms frequency transients, so that the unit will not trip |  |  |  |  |  |  |  | P |
| Note: <br> The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software. |  |  |  |  |  |  |  |  |  |


| 4.9.3 Requirements on voltage and frequency protection <br> 4.9.3.1 <br>  General (Interface protection: Over/under voltage) <br> (Setting value refer EN 50438 for default settings)  |  |  |  | P |
| :---: | :---: | :---: | :---: | :---: |
| Test conditions |  | Output power: 3,0kW Frequency: $50+/-0,2 \mathrm{~Hz}$ |  |  |
| Limit [V] | Trip value [V] | Voltage step [V] | Disconnection time [s] | Limit [s] |
| $\begin{aligned} & \text { Stage } 1 \\ & 110 \% \text { of } U_{n} \\ & =253,0 \end{aligned}$ | 252,9 | 230 to 258 | 2,010 | $\leq 3,0$ s |
|  | 252,9 | 230 to 258 | 2,010 |  |
|  | 252,9 | 230 to 258 | 2,015 |  |
|  | 252,9 | 230 to 258 | 2,010 |  |
|  | 252,9 | 230 to 258 | 2,010 |  |
| $\begin{gathered} \text { Stage } 2 \\ 115 \% \text { of } U_{n} \\ =264,5 \end{gathered}$ | 264,1 | 230 to 269 | 0,139 | $0,1 \mathrm{~s} \leq \mathrm{t} \leq 0,2 \mathrm{~s}$ |
|  | 264,1 | 230 to 269 | 0,121 |  |
|  | 264,1 | 230 to 269 | 0,139 |  |
|  | 264,1 | 230 to 269 | 0,139 |  |
|  | 264,1 | 230 to 269 | 0,140 |  |
| Stage <br> $85 \%$ of $U_{n}$ $=195,5$ | 195,3 | 230 to 190 | 1,298 | $1,2 \mathrm{~s} \leq \mathrm{t} \leq 1,5 \mathrm{~s}$ |
|  | 195,3 | 230 to 190 | 1,298 |  |
|  | 195,3 | 230 to 190 | 1,296 |  |
|  | 195,3 | 230 to 190 | 1,312 |  |
|  | 195,3 | 230 to 190 | 1,290 |  |

## Note:

The trip values were evaluated by varying the applied voltage from $U_{n}$ down to $U_{\text {th-low }}-2 \%$ of $U_{n}$ in steps of $0,5 \%$ of $U_{n}$ for under-voltage testing as well as from $U_{n}$ up to $U_{\text {th-high }}+2 \%$ of $U_{n}$ in steps of $0,5 \%$ of $U_{n}$ for overvoltage testing, Lower and upper threshold voltage shall not fall or rise below or above $2,3 \mathrm{~V}$ of the trip value itself, The disconnection time was measured by application of a negative voltage step from $U_{n}$ to the operate value $-5 \%$ of $U_{n}$ as well as positive voltage step from $U_{n}$ to the operate value $+5 \%$ of $U_{n}$.
The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.

## Scope pictures of the disconnection time

Over-voltage - Stage 1


Over-voltage - Stage 2


Under-voltage


| $\begin{aligned} & 4.9 .3 \\ & 4.9 .3 .1 \end{aligned}$ | Requirements on voltage and frequency protection General (Maximum voltage 10 min mean protection according to EN 50160) (Setting value refer EN 50438 for default settings) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Setting values of the protection: |  | Trip value Setting [V] | 253 |  |
|  |  | Setting $\mathrm{T}_{\text {disconnection trip value }}[\mathrm{s}$ ] | 600 |  |
|  |  | Setting $\mathrm{T}_{\text {disconnection }}$ [ms] | 200 |  |
| Test: |  |  |  |  |
|  |  | Disconnection time [s] | Limit [s] |  |
| a) | The voltage is set to $100 \% U_{n}$ and held for 600 s , Thereafter the voltage is set to $112 \% U_{n}$, Disconnection must take place within 600 s . |  |  |  |
|  | Phase 1: | 491 s | $\leq 600$ s |  |
|  | Phase 2: | N/A |  |  |
|  | Phase 3: | N/A |  |  |
| b) P | The voltage is set to $U_{n}$ for 600 s and then to $108 \% \mathrm{U}_{\mathrm{n}}$ for 600 s , No disconnection should take place |  |  |  |
|  | Phase 1: | No Disconnection | Disconnection should not take place, |  |
|  | Phase 2: | N/A |  |  |
|  | Phase 3: | N/A |  |  |
| c) | The voltage is set to $106 \% U_{n}$ and held for 600 s , Thereafter the voltage is set to $114 \% U_{n}$, The disconnection should last for half the period as in Point a)* |  |  |  |
|  | Phase 1: | 261 s | The disconnection time should about $50 \%$ of the value measur in a), * |  |
|  | Phase 2: | N/A |  |  |
|  | Phase 3: | N/A |  |  |
| Test: <br> a) This test serves as proof of the measurement accuracy and the maximum set time. <br> b) This test serves as proof of the measurement accuracy. <br> c) This test serves as proof of the correct formation of the 1 minute running mean value. |  |  |  |  |
| Assessment criterion: <br> The permitted tolerance between setting value and trip value of the voltage may not exceed $\pm 1$ <br> Limit values: <br> Rise-in voltage protection $1,1 \mathrm{U}_{\mathrm{N}}$ after a max. 600 s , the switch off after 200 ms . |  |  |  |  |
| Note: <br> If only one integrated protection is used for the power generation systems, the value of the rise-in voltage protection of $1,1 U_{N}$ may not be changed. <br> *If the setting value is set to 600 s , then the disconnection time can be in the range between 225 s and 375 s . The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software. |  |  |  |  |


b) Voltage set to $108 \% \mathrm{U}_{\mathrm{n}}$ :

c) Voltage set to $106 \% U_{n}$, thereafter $114 \% U_{n}$ :


| 4.9.3 Requirements on voltage and frequency protection <br> 4.9.3.1 General (Interface protection: Over/under frequency) <br>  (Setting value refer EN 50438 Default setting) |  |  |  | P |
| :---: | :---: | :---: | :---: | :---: |
| Test conditions | Output power: 3,0kW$\mathrm{U}_{\mathrm{n}}=230 \mathrm{Vac}$ |  |  |  |
|  | Under-frequency |  | Over-frequency |  |
| Parameter | Stage 1 <br> Under-Frequency | Time | Stage 1 Over-Frequency | Time |
| Limit | $47,50 \mathrm{~Hz}$ | $0,3 \leq \mathrm{t} \leq 0,5 \mathrm{~s}$ | $51,50 \mathrm{~Hz}$ | $0,3 \leq t \leq 0,5 \mathrm{~s}$ |
| Trip value [ Hz ] | 47,50 |  | 52,02 |  |
|  | 47,50 |  | 52,02 |  |
|  | 47,50 |  | 52,02 |  |
|  | 47,50 |  | 52,02 |  |
|  | 47,50 |  | 52,02 |  |
| Disconnection time [s] | $\begin{aligned} & 50,00 \mathrm{~Hz} \\ & \text { to } \\ & 47,40 \mathrm{~Hz} \end{aligned}$ | 0,410 | $\begin{aligned} & 50,00 \mathrm{~Hz} \\ & \text { to } \\ & 52,10 \mathrm{~Hz} \end{aligned}$ | 0,395 |
|  |  | 0,420 |  | 0,405 |
|  |  | 0,435 |  | 0,405 |
|  |  | 0,435 |  | 0,420 |
|  |  | 0,435 |  | 0,420 |

## Note:

For under-frequency testing the applied frequency is varied from $f_{n}$ down to $f_{\text {th-low }}-0,1 \mathrm{~Hz}$ in steps of $0,025 \mathrm{~Hz}$ with a time duration per step exceeding the configured disconnection time, The operate value is the value of the applied frequency at switch the protection function trips and shall be within $f_{t h-l o w} \pm 0,05 \mathrm{~Hz}$.

For over-frequency testing the applied frequency is varied from $f_{n}$ up to $f_{\text {th-high }}+0,1 \mathrm{~Hz}$ in steps of $0,025 \mathrm{~Hz}$ with a time duration per step exceeding the configured disconnection time, The operate value is the value of the applied frequency at which the protection function trips and shall be within $f_{t h-h i g h} \pm 0,05 \mathrm{~Hz}$.

The disconnection time was measured by applying a negative or positive frequency ramp from $f_{n}$ to the operate value $-0,1 \mathrm{~Hz}$ or $+0,1 \mathrm{~Hz}, \mathrm{e}, \mathrm{g}$, from 50 Hz to $47,4 \mathrm{~Hz}$, The time elapsed between the application of the frequency ramp and the opening of the interface switch was calculated by the measured time minus the 2500 ms from $50,0 \mathrm{~Hz}$ to $47,5 \mathrm{~Hz}$.
The oscilloscope pictures below show the measured worst case disconnection times.
The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.



| Load imbalance (real, reactive load) for test condition A (EUT output = 100\%) |  |  |  |  |  |  |  |  |  | P |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Test : |  |  |  |  |  |  |  |  |  |  |
| Test conditions |  |  | $\begin{gathered} \text { Frequency: } 50+/-0,1 \mathrm{~Hz} \\ U_{N}=230+/-3 \mathrm{Vac} \\ \text { Distortion factor of chokes }<2 \% \\ \text { Quality }=1 \end{gathered}$ |  |  |  |  |  |  |  |
| Disconnection limit |  |  | 2 s (IEC 62116) |  |  |  |  |  |  |  |
| No | $\begin{aligned} & \text { PEUT }^{1)} \\ & \text { [\% of EUT } \\ & \text { rating] } \end{aligned}$ | Reactive Ioad [\% of QL in 6,1,d) ${ }^{1)}$ | $\begin{gathered} \mathrm{P}_{\mathrm{AC}}{ }^{2)} \\ {[\% \text { of }} \\ \text { nominal] } \end{gathered}$ | $\begin{gathered} \mathrm{QAC}^{3)} \\ {[\% \text { of }} \\ \text { nominal] } \end{gathered}$ | $\begin{gathered} \mathrm{IAC}^{4)} \\ {[\mathrm{A}]} \end{gathered}$ | Peut [kW per phase] | VDC [V] | Qf | Run on Time [ms] | Remarks <br> 5) |
| 1 | 100 | 100 | 0 | 0 | 0,020 | 3,000 | 368 | 0,999 | 326 | BL |
| 2 | 100 | 100 | -5 | -5 | 0,671 | 3,000 | 368 | 1,025 | 223 | IB |
| 3 | 100 | 100 | -5 | 0 | 0,642 | 3,000 | 368 | 1,052 | 277 | IB |
| 4 | 100 | 100 | -5 | +5 | 0,576 | 3,000 | 368 | 1,078 | 314 | IB |
| 5 | 100 | 100 | 0 | -5 | 0,021 | 3,000 | 368 | 0,974 | 223 | IB |
| 6 | 100 | 100 | 0 | +5 | 0,111 | 3,000 | 368 | 1,024 | 308 | IB |
| 7 | 100 | 100 | +5 | -5 | 0,674 | 3,000 | 368 | 0,928 | 218 | IB |
| 8 | 100 | 100 | +5 | 0 | 0,700 | 3,000 | 368 | 0,952 | 306 | IB |
| 9 | 100 | 100 | +5 | +5 | 0,759 | 3,000 | 368 | 0,975 | 317 | IB |
| Parameter at 0\% per phase |  |  | $\mathrm{L}=33,68 \mathrm{mH}$ |  |  | $R=10,58 \Omega$ |  | $\mathrm{C}=300,86 \mu \mathrm{~F}$ |  |  |

## Note:

RLC is adjusted to min. +/-1\% of the inverter rated output power

1) Peut: EUT output power.
2) Pac: Real power flow at S 1 in Figure 1. Positive means power from EUT to utility, Nominal is the $0 \%$ test condition value.
${ }^{3)}$ Qac: Reactive power flow at S1 in Figure 1. Positive means power from EUT to utility, Nominal is the 0 \% test condition value.
3) Fundamental of $I_{A C}$ when RLC is adjusted.
${ }^{5)}$ BL: Balance condition, IB: Imbalance condition.
Condition A:
EUT output power $\mathrm{P}_{\text {EUT }}=$ Maximum ${ }^{6}$
EUT input voltage ${ }^{6)}=>75 \%$ of rated input voltage range
${ }^{6)}$ Maximum EUT output power condition should be achieved using the maximum allowable input power, Actual output power may exceed nominal rated output.
${ }^{7}$ ) Based on EUT rated input operating range, For example, If range is between $X$ volts and $Y$ volts, $75 \%$ of range $=X+0,75 \times(Y-X), Y$ shall not exceed $0,8 \times$ EUT maximum system voltage (i,e,, maximum allowable array open circuit voltage), In any case, the EUT should not be operated outside of its allowable input voltage range.
The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.


| Load imbalance (reactive load) for test condition B (EUT output = 50 \% - 66 \%) |  |  |  |  |  |  |  |  |  | P |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Test : |  |  |  |  |  |  |  |  |  |  |
| Test conditions |  |  | $\begin{gathered} \text { Frequency: } 50+/-0,1 \mathrm{~Hz} \\ U_{N}=230+/-3 \mathrm{Vac} \\ \text { Distortion factor of chokes }<2 \% \\ \text { Quality }=1 \end{gathered}$ |  |  |  |  |  |  |  |
| Disconnection limit |  |  | 2s (IEC 62116) |  |  |  |  |  |  |  |
| No | $\begin{aligned} & \text { Peut }{ }^{1)} \\ & \text { [\% of EUT } \\ & \text { rating] } \end{aligned}$ | Reactive load [\% of QL in 6,1,d) ${ }^{1)}$ | $\begin{gathered} \mathrm{P}_{\mathrm{AC}}{ }^{2)} \\ {[\% \text { of }} \\ \text { nominal] } \end{gathered}$ | $\begin{gathered} \mathrm{QAC}^{3)} \\ {[\% \text { of }} \\ \text { nominal] } \end{gathered}$ | $\begin{gathered} \mathrm{IAC}^{4)} \\ {[\mathrm{A}]} \end{gathered}$ | Peut [kW per phase] | VDC [V] | Qf | Run on Time [ms] | Remarks <br> 5) |
| 1 | 66 | 66 | 0 | -5 | 0,026 | 1,980 | 272 | 0,975 | 212 | IB |
| 2 | 66 | 66 | 0 | -4 | 0,024 | 1,980 | 272 | 0,980 | 231 | IB |
| 3 | 66 | 66 | 0 | -3 | 0,022 | 1,980 | 272 | 0,985 | 238 | IB |
| 4 | 66 | 66 | 0 | -2 | 0,022 | 1,980 | 272 | 0,990 | 242 | IB |
| 5 | 66 | 66 | 0 | -1 | 0,022 | 1,980 | 272 | 0,995 | 287 | IB |
| 6 | 66 | 66 | 0 | 0 | 0,022 | 1,980 | 272 | 1,000 | 432 | BL |
| 7 | 66 | 66 | 0 | +1 | 0,026 | 1,980 | 272 | 1,005 | 418 | IB |
| 8 | 66 | 66 | 0 | +2 | 0,029 | 1,980 | 272 | 1,010 | 376 | IB |
| 9 | 66 | 66 | 0 | +3 | 0,033 | 1,980 | 272 | 1,015 | 361 | IB |
| 10 | 66 | 66 | 0 | +4 | 0,038 | 1,980 | 272 | 1,020 | 318 | IB |
| 11 | 66 | 66 | 0 | +5 | 0,043 | 1,980 | 272 | 1,025 | 300 | IB |
| Parameter at 0\% per phase |  |  | $\mathrm{L}=51,27 \mathrm{mH}$ |  |  | $R=16,11 \Omega$ |  | $\mathrm{C}=197,60 \mu \mathrm{~F}$ |  |  |

## Note:

RLC is adjusted to min. +/-1\% of the inverter rated output power

1) Peut: EUT output power.
2) ${ }^{\text {2 }}$ Ac: Real power flow at S 1 in Figure 1, Positive means power from EUT to utility, Nominal is the $0 \%$ test condition value.
 test condition value.
3) Fundamental of $\mathrm{l}_{\mathrm{AC}}$ when RLC is adjusted.
${ }^{5)}$ BL: Balance condition, IB: Imbalance condition.
Condition B:
EUT output power $P_{\text {EUT }}=50 \%-66 \%$ of maximum
EUT input voltage ${ }^{6)}=50 \%$ of rated input voltage range, $\pm 10 \%$
${ }^{6)}$ Based on EUT rated input operating range, For example, If range is between $X$ volts and $Y$ volts, $50 \%$ of range $=\mathrm{X}+0,5 \times(\mathrm{Y}-\mathrm{X})$, Y shall not exceed $0,8 \times$ EUT maximum system voltage (i,e,, maximum allowable array open circuit voltage), In any case, the EUT should not be operated outside of its allowable input voltage range.
The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.


| Load imbalance (reactive load) for test condition C (EUT output = 25 \% - 33 \%) |  |  |  |  |  |  |  |  |  | P |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Test : |  |  |  |  |  |  |  |  |  |  |
| Test conditions |  |  | $\begin{gathered} \text { Frequency: } 50+/-0,1 \mathrm{~Hz} \\ U_{N}=230+/-3 \mathrm{Vac} \\ \text { Distortion factor of chokes }<2 \% \\ \text { Quality }=1 \end{gathered}$ |  |  |  |  |  |  |  |
| Disconnection limit |  |  | 2s (IEC 62116) |  |  |  |  |  |  |  |
| No | $\begin{aligned} & \text { Peut }{ }^{1)} \\ & \text { [\% of EUT } \\ & \text { rating] } \end{aligned}$ | Reactive load [\% of QL in 6,1,d) ${ }^{1)}$ | $\mathrm{PAC}^{2)}$ <br> [\% of nominal] | $\begin{gathered} \mathrm{QAC}^{3)} \\ {[\% \text { of }} \\ \text { nominal] } \end{gathered}$ | $\begin{gathered} \mathrm{IAC}^{4)} \\ {[\mathrm{A}]} \end{gathered}$ | Peut [kW per phase] | VDC [V] | Qf | Run on Time [ms] | Remarks <br> 5) |
| 1 | 33 | 33 | 0 | -5 | 0,022 | 990 | 157 | 0,975 | 215 | IB |
| 2 | 33 | 33 | 0 | -4 | 0,021 | 990 | 157 | 0,980 | 226 | IB |
| 3 | 33 | 33 | 0 | -3 | 0,020 | 990 | 157 | 0,985 | 234 | IB |
| 4 | 33 | 33 | 0 | -2 | 0,020 | 990 | 157 | 0,990 | 249 | IB |
| 5 | 33 | 33 | 0 | -1 | 0,020 | 990 | 157 | 0,995 | 277 | IB |
| 6 | 33 | 33 | 0 | 0 | 0,020 | 990 | 157 | 1,000 | 308 | BL |
| 7 | 33 | 33 | 0 | +1 | 0,022 | 990 | 157 | 1,005 | 441 | IB |
| 8 | 33 | 33 | 0 | +2 | 0,024 | 990 | 157 | 1,010 | 396 | IB |
| 9 | 33 | 33 | 0 | +3 | 0,025 | 990 | 157 | 1,015 | 378 | IB |
| 10 | 33 | 33 | 0 | +4 | 0,028 | 990 | 157 | 1,020 | 366 | IB |
| 11 | 33 | 33 | 0 | +5 | 0,031 | 990 | 157 | 1,025 | 357 | IB |
| Parameter at 0\% per phase |  |  | $\mathrm{L}=103,94 \mathrm{mH}$ |  |  | $\mathrm{R}=32,65 \Omega$ |  | $\mathrm{C}=97,48 \mu \mathrm{~F}$ |  |  |

## Note:

RLC is adjusted to min. $+/-1 \%$ of the inverter rated output power

1) PEUT: EUT output power.
${ }^{\text {2) }}$ Pac: Real power flow at S 1 in Figure 1, Positive means power from EUT to utility, Nominal is the $0 \%$ test condition value.
 test condition value.
2) Fundamental of $\mathrm{l}_{\mathrm{AC}}$ when RLC is adjusted.
${ }^{5)}$ BL: Balance condition, IB: Imbalance condition.
Condition B:
EUT output power $\mathrm{P}_{\text {EUT }}=25 \%-33 \%{ }^{6}$ ) of maximum
EUT input voltage ${ }^{7 \text { ) }}=<20 \%$ of rated input voltage range
${ }^{6)}$ Or minimum allowable EUT output level if greater than $33 \%$.
${ }^{7}$ ) Based on EUT rated input operating range, For example, If range is between $X$ volts and $Y$ volts, $20 \%$ of range $=\mathrm{X}+0,2 \times(\mathrm{Y}-\mathrm{X})$, Y shall not exceed $0,8 \times \mathrm{EUT}$ maximum system voltage ( $\mathrm{i}, \mathrm{e}$, , maximum allowable array open circuit voltage), In any case, the EUT should not be operated outside of its allowable input voltage range.
The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.


EN 50549-1:2019: Connection and starting to generate electrical power

| Clause | Test requirement | Test procedure according standard | Result |
| :--- | :--- | :--- | :---: |
| 4.10 .2 | Automatic reconnection after trippin | EN 50438, Annex D.3.6 | P |
| 4.10 .3 | Starting to generate electrical power | EN 50438, Annex D.3.6 | P |



|  | Frequency conditions |  |
| :---: | :---: | :---: |
| d) Start up for frequency range | $<49,50 \mathrm{~Hz}$ for twice of setting observation time | $>50,10 \mathrm{~Hz}$ for twice of setting observation time |
| Connection: | No connection | No connection |
| Limit | No connection allowed |  |
| e) In frequency range at start-up | $\geq 49,50 \mathrm{~Hz}$ within twice of setting observation time | $\leq 50,10 \mathrm{~Hz}$ within twice of setting observation time |
| Reconnection time [s] | 68 s | 67 s |
| Limit: | Connected after setting delay time( $\geq 60 \mathrm{~s}$ ) |  |
| Gradient: | The maximum occurring active power gradient after connection respectively start generating electrical power is less than the configured maximum active power per minute Max gradient: disable. For recorded gradient see diagram below. |  |
| f) In frequency range after frequency failture | $\geq 49,50 \mathrm{~Hz}$ for twice of setting observation time | $\leq 50,20 \mathrm{~Hz}$ for twice of setting observation time |
| Reconnection time [s] | 68 s | 68 s |
| Limit: | Reconnection after setting observation time ( $\geq 60$ s) |  |
| Gradient: | For adjustable micro generators the maximum occurring active power gradient after connection respectively start generating electrical power is less than the configured maximum active power per minute Max gradient: 10\%PEmax/min. <br> For non or partly adjustable generators the connection after trip of the interface protection is delayed by a randomised value between 1 min and 10 min . <br> For recorded gradient see diagram below. |  |
| Test: <br> Test condition b) and c): voltage withi Test condition e): frequency within the Test condition f): frequency within the <br> In order to avoid continuous starting disengaging value of frequency and <br> The test had been performed on the ASW1500S-S, ASW2000S-S since it | he limits of $85 \%$ to $110 \% U_{n}$. mits of $49,50 \mathrm{~Hz}$ to $50,1 \mathrm{~Hz}$. mits of $49,50 \mathrm{~Hz}$ to $50,2 \mathrm{~Hz}$. <br> disengaging operations of the inte age functions shall be above $2 \%$ del ASW3000S-S, the test results identical in hardware and software. | ace protection relay, the viating from the operate value. valid for the ASW1000S-S, |
| Assessment criterion: <br> a) the micro generator connects respe permitted range of voltage and freque b) for adjustable micro generators the respectively start generating electrical power per minute and <br> c) for non or partly adjustable generat delayed by a randomised value betwe | ively starts generating electrical po $y$ and aximum occurring active power gr ower is less than the configured maxi <br> the connection after trip of the int 1 min and 10 min . | er only in the <br> ient after connection imum active <br> face protection is |

Graph of the gradual power supply : Test b) for $\geq 85 \% U_{n}$


Graph of the gradual power supply : Test b) for $\leq 110 \% U_{n}$


Graph of the gradual power supply : Test c) for $\geq 85 \% U_{n}$


Graph of the gradual power supply : Test c) for $\leq 110 \% U_{n}$



Graph of the gradual power supply : Test e) for $\leq 50,10 \mathrm{~Hz}$


Graph of the gradual power supply : Test f) for $\geq 49,50 \mathrm{~Hz}$


Graph of the gradual power supply : Test f) for $\leq 50,20 \mathrm{~Hz}$


EN 50549-1:2019: Ceasing and reduction of active power on set point

| Clause | Test requirement | Test procedure according standard | Result |
| :--- | :--- | :--- | :---: |
| 4.11 .1 | Ceasing active power | CEI 0-21:2019-04, Annex A.4.3.3.2 | P |
| 4.11 .2 | Reduction of active power on a set point | FGW TG3, Revision 25, clause 4.1.2 | P |


| 4.11.1 Ceasing active power | P |
| :--- | :--- | :---: |
| Operating time of the monitoring device |  |
| Test: | Remote tripping signal for the external disconnection |
| Limit [s]: | 5 s |
| Reaction time of the tripping <br> value [s]: | $0,039 \mathrm{~s}$ |

## Note:

The test method refer to Annex A,4,3,2 of CEI 0-21:2019-04,
Generating plants shall be equipped with a logic interface (input port) in order to cease active power output within five seconds following an instruction being received at the input port, If required by the DSO, this includes remote operation.
The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.


| 4.11.2 Reduction of active power on set point |  |  |  | P |
| :---: | :---: | :---: | :---: | :---: |
| Test result: |  |  |  |  |
| Setpoint power bin [\%PEmax] | $\mathrm{P}_{\text {set }}[\mathrm{kW}$ ] | $\mathrm{P}_{60}[\mathrm{~kW}]$ | Deviation [\%P $\mathrm{Emax}^{\text {m }}$ ] |  |
| 100\% | 3,000 | 3,004 | 0,144 |  |
| 90\% | 2,700 | 2,714 | 0,451 |  |
| 80\% | 2,400 | 2,406 | 0,190 |  |
| 70\% | 2,100 | 2,101 | 0,039 |  |
| 60\% | 1,800 | 1,799 | -0,045 |  |
| 50\% | 1,500 | 1,495 | -0,167 |  |
| 40\% | 1,200 | 1,204 | 0,132 |  |
| 30\% | 0,900 | 0,898 | -0,075 |  |
| 20\% | 0,600 | 0,591 | -0,294 |  |
| 10\% | 0,300 | 0,284 | -0,519 |  |
| 5\% | 0,150 | 0,140 | -0,328 |  |
|  | Setpoint power bin [\%PEmax] |  | Deviation[\%P Emax] |  |
| Max. deviation | 10\% |  | -0,519 |  |
| Limit $\Delta \mathrm{P}_{\text {E60 }} / \mathrm{P}_{\text {Setpoint }}$ : | + $5 \%$ of $\mathrm{P}_{\text {Emax }}$ |  |  |  |

## Test:

The setpoint signal must be reduced from $100 \%$ to 0\% Pemax:
a) for adjustable PGUs in increments of $10 \%$ Pemax, 1 minute must elapse after every change to the setpoint setting so that the PGU can settle at the new setpoint, Then the active power of the PGU must be measured as a 1 -min mean value.
b) For all other PGUs, in line with their adjustable steps, 5 minutes must elapse after the setpoint setting is changed so that the PGU can settle at the new setpoint, Then the active power of the PGU must be measured as a 1 -min mean value.

## Assessment criterion:

a) for adjustable PGUs:

- no network disconnection
- the active power value does not exceed the setpoint by more than $5 \% \mathrm{P}_{\mathrm{Emax}}$
- the setting time determined this way is $\leq 1 \mathrm{~min}$
b) For all other PGUs:
- the active power value does not exceed the setpoint by more than $5 \% \mathrm{PEmax}$ or
- the setpoint is fallen below within 5 minutes or the PGU has switched off


## Note:

The setting time is $\leq 1 \mathrm{~min}$. See below "Graph of the setting accuracy".
The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software.


## EN 50549-1:2019

| Clause | Test requirement | Test procedure according standard | Result |
| :--- | :--- | :--- | :---: |
| 4.13 | Requirements regarding single fault <br> tolerance of interface protection system <br> and interface switch | VDE V 0124-100:2019-02 (Draft), clause <br> 5.5 .2 | $\mathbf{P}$ |


| 4.13 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :--- | :--- |
| Requirements regarding single fault tolerance of interface protection |
| system and interface switch |


| Component No. | Fault | Test condition |  | Test time | Fuse No, | Fault condition |  | Result |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AC | DC |  |  | AC | DC |  |
| DC isolation device function detector (R615) | 0-C <br> before start up | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | 30 min | - | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | The PCE didn't start. Error 38 ISO check fail. No harzard happened. |
| Residual current detector (R275) | O-C | $\begin{aligned} & 230 \mathrm{~V} \\ & 13,1 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 380 \mathrm{~V} \\ & 7,9 \mathrm{~A} \end{aligned}$ | 30 min | - | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | The PCE shut down.The PCE didn't start. Error 9 GFCI check fail. No harzard happened. |
| Residual current detector (R226 ) | O-C | $\begin{aligned} & 230 \mathrm{~V} \\ & 13,1 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 380 \mathrm{~V} \\ & 7,9 \mathrm{~A} \end{aligned}$ | 30 min | - | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | The PCE shut down.The PCE didn't start. Error 9 GFCI check fail. No harzard happened. |
| Residual current detector (R227) | O-C | $\begin{aligned} & 230 \mathrm{~V} \\ & 13,1 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 380 \mathrm{~V} \\ & 7,9 \mathrm{~A} \end{aligned}$ | 30 min | - | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | The PCE shut down.The PCE didn't start. Error 9 GFCI check fail. No harzard happened. |
| Residual current detector (R228 ) | O-C | $\begin{aligned} & 230 \mathrm{~V} \\ & 13,1 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 380 \mathrm{~V} \\ & 7,9 \mathrm{~A} \end{aligned}$ | 30 min | - | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | The PCE shut down.The PCE didn't start. Error 9 GFCl check fail. No harzard happened. |
| Relay 201 | S-C <br> before start up | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | 30 min | - | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | The PCE didn't start. Error 3 Relay check fail. No harzard happened. |
| Relay 202 | s-C <br> before start up | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | 30 min | - | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | The PCE didn't start. Error 3 Relay check fail. No harzard happened. |
| Relay 203 | s-c <br> before start up | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | 30 min | - | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | The PCE didn't start. Error 3 Relay check fail. No harzard happened. |
| Relay 204 | s-c <br> before start up | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | 30 min | - | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | The PCE didn't start. Error 3 Relay check fail. No harzard happened. |
| Relay function detector (Q405 D-S) | S-C | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | 30 min | - | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | The PCE didn't start. Error 3 Relay check fail. No harzard happened. |
| Inverter drive (R301) | O-C | $\begin{aligned} & 230 \mathrm{~V} \\ & 13,1 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 380 \mathrm{~V} \\ & 7,9 \mathrm{~A} \end{aligned}$ | 30 min | - | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | The PCE shut down.The PCE didn't start.Error 4 DCI protestion. No harzard happened. |
| Inverter drive (R309) | O-C | $\begin{aligned} & 230 \mathrm{~V} \\ & 13,1 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 380 \mathrm{~V} \\ & 7,9 \mathrm{~A} \end{aligned}$ | 30 min | - | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | The PCE shut down.The PCE didn't start.Error 4 DCI protestion. No harzard happened. |


| Component No. | Fault | Test condition |  | Test time | Fuse No, | Fault condition |  | Result |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AC | DC |  |  | AC | DC |  |
| Inverter drive (R313) | O-C | $\begin{aligned} & 230 \mathrm{~V} \\ & 13,1 \mathrm{~A} \end{aligned}$ | $\begin{gathered} 380 \mathrm{~V} \\ 7,9 \mathrm{~A} \end{gathered}$ | 30 min | - | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | The PCE shut down.The PCE didn't start.Error 4 DCI protestion. No harzard happened. |
| Main CPU oscillator (R749) | S-C | $\begin{aligned} & 230 \mathrm{~V} \\ & 13,1 \mathrm{~A} \end{aligned}$ | $\begin{gathered} 380 \mathrm{~V} \\ 7,9 \mathrm{~A} \end{gathered}$ | 30 min | - | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | The PCE shut down.The PCE didn't start.No error code. No harzard happened. |
| MainCPU and slave CPU communication (R792) | O-C | $\begin{aligned} & 230 \mathrm{~V} \\ & 13,1 \mathrm{~A} \end{aligned}$ | $\begin{gathered} 380 \mathrm{~V} \\ 7,9 \mathrm{~A} \end{gathered}$ | 30 min | - | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | The PCE shut down.The PCE didn't start.No error code. No harzard happened. |
| MainCPU and slave CPU communication (R765) | O-C | $\begin{aligned} & 230 \mathrm{~V} \\ & 13,1 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 380 \mathrm{~V} \\ & 7,9 \mathrm{~A} \end{aligned}$ | 30 min | - | $\begin{aligned} & 230 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 487 \mathrm{~V} \\ & 0,01 \mathrm{~A} \end{aligned}$ | The PCE shut down.The PCE didn't start. No error code. No harzard happened. |
| The errors in the control circuit simulate that the safety is even under one error ensured, |  |  |  |  |  |  |  |  |
| Addendum - Shutdown device |  |  |  |  |  |  |  |  |
| Each active phase can be switched, ( L and N ) |  |  |  |  |  |  |  | Yes |
| If no galvanic separation between AC and DC (PV): <br> Two relays in series on each active phase are necessary to fulfil the basic insulation or simple separation based on the PV working voltage, |  |  |  |  |  |  |  | Two relays in series on each active phase |
| Note: <br> The test had been performed on the model ASW3000S-S, the test results are valid for the ASW1000S-S, ASW1500S-S, ASW2000S-S since it is identical in hardware and software. |  |  |  |  |  |  |  |  |

## Annex No. 3

Pictures of the unit


## Enclosure Bottom view



Enclosure top view


## Enclosure side view-1



Enclosure side view-2


## Internal view 1



Internal view 2


Main board -component side view


Main board-solder side view


## Annex No. 4

## Test Equipment list

Date(s) of performance test: 2019-12-10 to 2020-01-08

| Equipment | Internal No, | Manufacturer | Type | Serial No, | Calibration is valid to |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Power analyzer | SCGJ296 | YOKOGAWA | WT1800 | // | Feb. 14, 2020 |
| Oscilloscope | SCGJ417 | YOKOGAWA | DLM2024 | // | Feb. 14, 2020 |
|  | SCGT208 | Agilent | DSO7014B | // | Feb. 14, 2020 |
| AC Source | 656038001333 | CHROMA | 6560 | // | Monitored by Power analyzer |
| DC Simulation Power supply | 62150EF01095 | CHROMA | $62150 \mathrm{H}-1000 \mathrm{~S}$ | // |  |
|  | 62150EF01095 | CHROMA | 62150H-600S | // |  |
| RLC load | 93V002581 | Qunling | ACTL-3803H | // |  |
| AC/DC Current probel | ZSCGJ0161 | Tektronix | A622 | // | Feb. 14, 2020 |
| Differential probel | P5200A | Tektronix | P5200A | // | Feb. 14, 2020 |
| Multi-meter | SCGJ334 | Fluke | F287 | // | Feb. 14, 2020 |

